

Parachute Materials and Stress Analysis

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Parachute Seminar

**3rd International Planetary Probe
Workshop**

Definitions

- **Fiber** - slender, threadlike structure; “tiny microscopic beams”
- **Filament** - a man-made fiber having great length compared to natural fibers
- **Staple** - a measure of length and/or fineness of a fiber
- **Yarn** - a generic term for continuous strands of textile staple fibers or continuous filaments in a form suitable for knitting, weaving, or otherwise intertwining to form a textile structure.

Definitions (continued)

- **Denier** - term used to describe the weight and size of a fiber or yarn (weight in grams of 9000 meters of material). Difficult to measure diameter of fibers.
- **Tex** - term found more commonly in Europe - grams per 1000 meters of yarn
- **Selvage** - specially woven edge that prevents the fabric from raveling (or unraveling)

Definitions (continued)

- **Tenacity** - strength of the fiber or yarn (units are grams per denier, gpd). Higher tenacity yarns must be of smaller denier to maintain adequate flexibility for weaving.

Denier = weight (in grams) of 9000m of yarn

= Volume X Specific Gravity (S.G.)

= 9000m X 10² cm/m X A (cm²) X S.G.

Tenacity = g/d = g/[9*10⁵ cm X A (cm²) X S.G.]

Solving for Force vs. Area (stress)

Stress @ Break = g/A (g/cm²) = 9*10⁵ cm X Tenacity X S.G.

= F/A (psi) = 12,800 X specific gravity X tenacity (gpd)

Stress @ Break (psi) = 12,800 X specific gravity X tenacity (gpd)

Definitions (continued)

- **Warp** - refers to the direction in a fabric, tape or webbing that run in the length-wise direction when coming off the loom.
- **Fill** - refers to the direction perpendicular to the “Warp” direction. (Also referred to as the “weft” or “woof”).
- **Picks per inch** - a measure of the yarn density in given direction (Warp or Fill) - number of threads per inch.
- **Fiber translation efficiency** - the ratio of the strength of the woven material to the total strength of the warp yarns.

Types of Materials

- **Natural**

- Wool
- *Silk*
- *Cotton*
- Hemp
- Flax
- Others

- **Man-made**

- Mineral Fibers
 - + *Glass*
 - + *Metal*
- Organic Fibers
 - + *Rayon*
 - + *Nylon*
 - + Dacron
 - + *Teflon*
 - + *Nomex*
 - + *Kevlar*
 - + *Spectra*
 - + *Vectran*
 - + *Zylon*

Nylon

- **Developed shortly before WWII**
- **A primary parachute material (Nylon 6-6)**
- **Polyamide resin with high tenacity due to long highly oriented molecules and high intermolecular forces**
- **Tenacity is 2.5 to 9.5 grams/denier (6.6 for Nylon 6-6)**
 - Stress @ Break (psi) = 12,800 X specific gravity X tenacity (gpd)**
= 12,800 X 1.14 X 6.6 = 96 ksi
- **Minimum elongation specified as 20%, actual elongation 30-40% at break**
- **Sensitive to ultraviolet light**
- **Does not burn readily, but melts at 480F**

Dacron

- **Polyester based man-made fiber**
- **Similar to nylon, but requires more treatment for stability**
- **Slightly lower elongation than nylon**
- **Better temperature resistance than nylon**
- **Slightly less weight and volume for comparable strength nylon, once making it attractive in sport parachutes**

Polytetrafluoroethylene, PTFE

- **Teflon (DuPont), Fluor (ICI)**
- **Fluorocarbon based man-made fiber**
- **Very low friction coefficient**
- **Very expensive**
- **Used for deployment bag liners**
- **Used as buffer material where cotton cannot be used**
- **Expanded PTFE (Goretex) available as a slit film fiber with a tenacity of 3 grams per denier**

Nomex

- **Polyamide man-made fiber**
- **Moderate tenacity of 5.4 grams per denier -> 90 ksi (s.g. = 1.38)**
- **Elongation at break about 16%**
- **Retains 50% of its strength at 500 F**
- **Used for flight suits and high-temperature buffers**
- **Has been used as cloth in parachutes in high temperature environments (e.g. F111 CEM stabilization parachute)**

Kevlar

- **High strength, high modulus, para-aramid fiber developed for use in radial tires**
- **Version used for parachute materials identified as “Intermediate Modulus Para-Aramid”**
- **Each fiber is 0.00047 inches in diameter and is approximately 1.5 denier**
- **Tenacity is quoted to be 20-22 grams per denier -> 370 ksi! (s.g.=1.44) (Mild Steel ~100 ksi)**
- **Elongation at break is 3-5%**
- **Does not melt or burn, but sensitive to UV**
- **Abrasion resistant, but is very abrasive itself**
- **Cannot be hot cut or have the bitter ends seared**

Spectra

- **High-strength polyethylene fiber**
- **Tenacity 30-35 grams per denier -> 380-440 ksi !!!**
- **Elongation at break is 2.7%**
- **Subject to loss of strength at temperature (10 g/d @ 212 F)**
- **Low coefficient of friction**
- **Sometimes difficult to get good seam efficiencies**
- **Used extensively in sport parachutes for suspension lines**
- **Becoming common as a deployment bag material for high density packs**
- **For more information see**
[***http://www.performancefibers.com/products/spectra.html***](http://www.performancefibers.com/products/spectra.html)

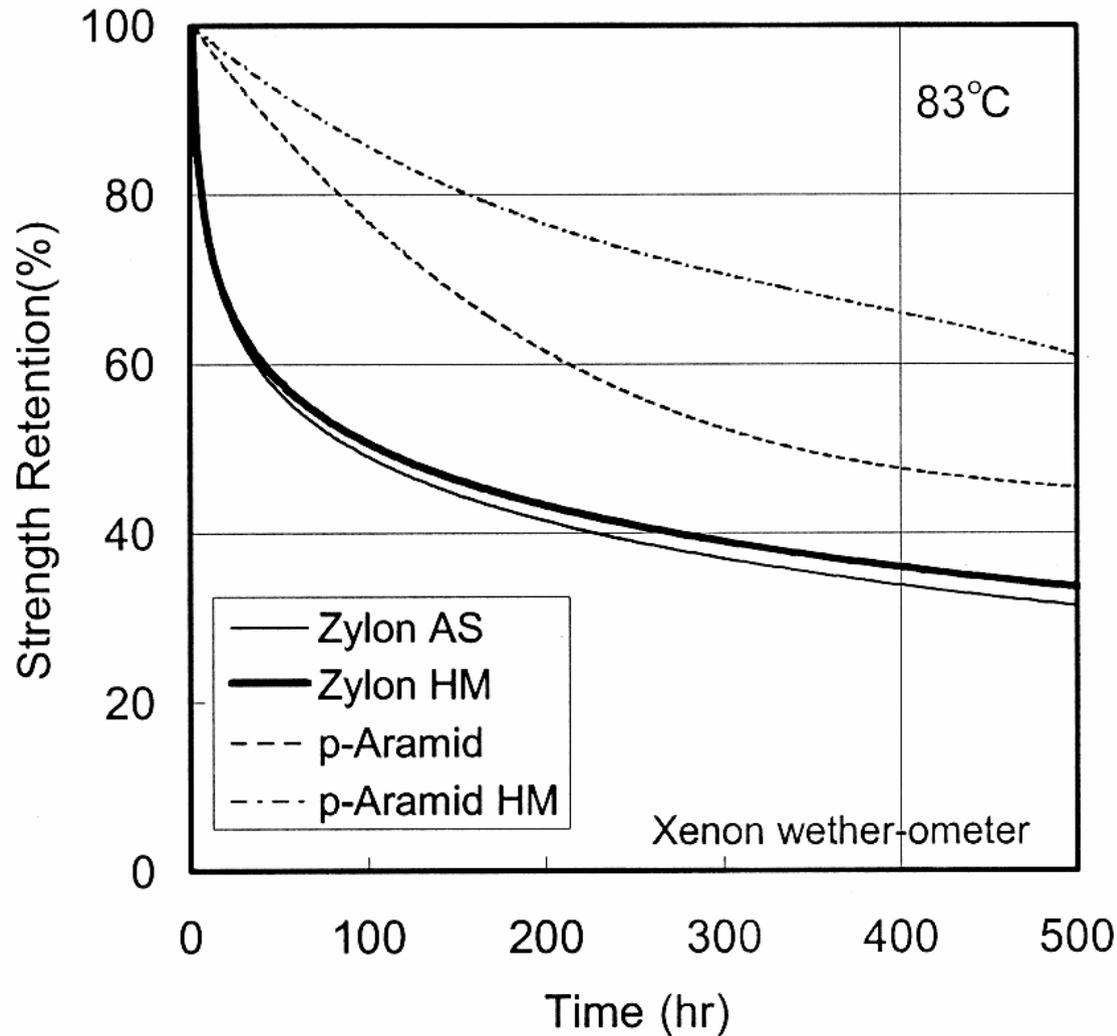
Vectran-LCP

- **LCP - Liquid Crystal Polymer**
- **Tenacity- 23 g/d => tensile strength = 300 ksi**
- **Elongation - 2-3%**
- **Friction properties similar to Spectra**
- **Immune to acids and UV**
- **Specific Gravity slightly less than 1.0**
- **Experiences zero creep under constant load**
- **Just entering the field of parachutes**

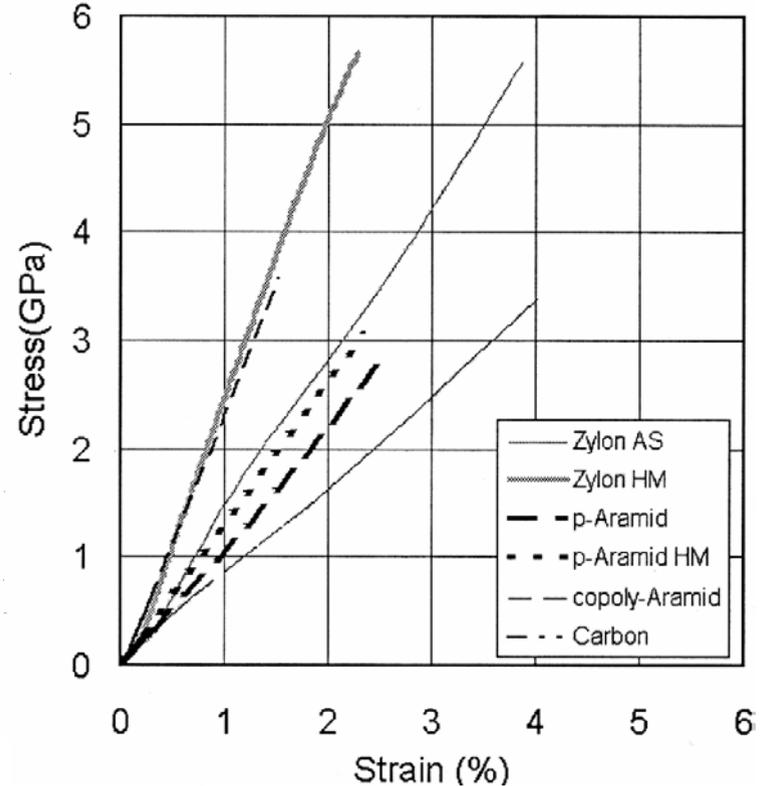
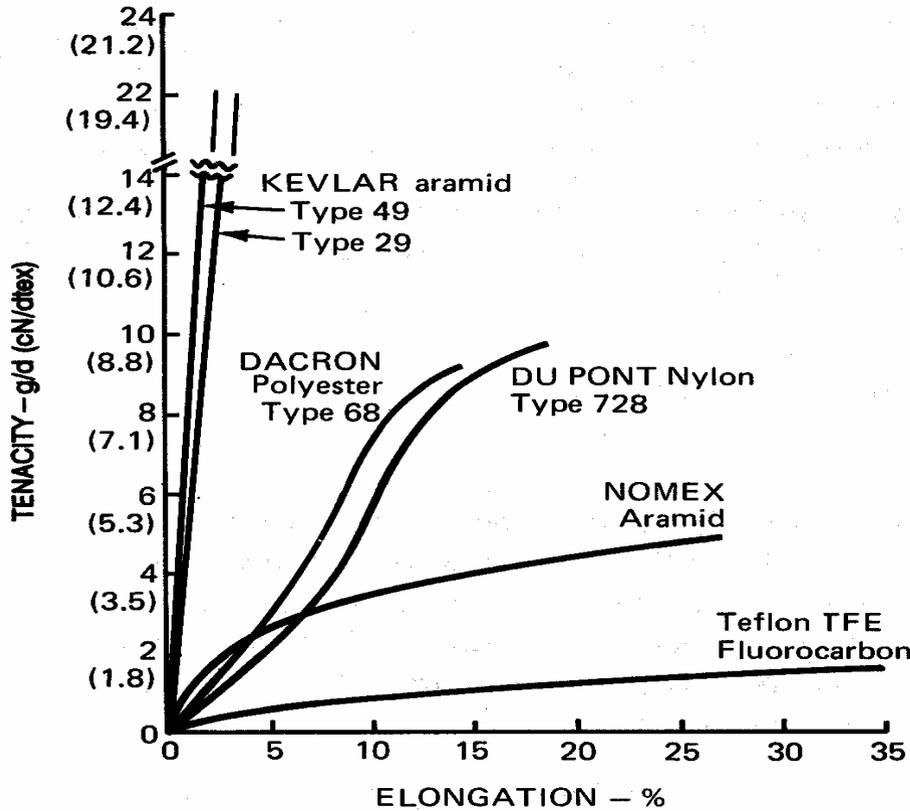
Zylon

- New fiber from TOYOBA (Japanese firm)
- “Rigid-rod chain molecules of poly(p-phenylene-2,6-benzobisoxazole) (PBO)”
- Tenacity - 43 gpd => 840 Ksi !!!
- Elongation at break - 3.5/2.5
- “Decomposition Temperature in Air” - 650 °C
- Much lower friction coefficient than Kevlar
- *Significant strength reductions with prolonged exposure to light (65% reduction in 6 months)*
- For more info see <http://www.toyobo.co.jp/e/seihin/kc/pbo/main.html>

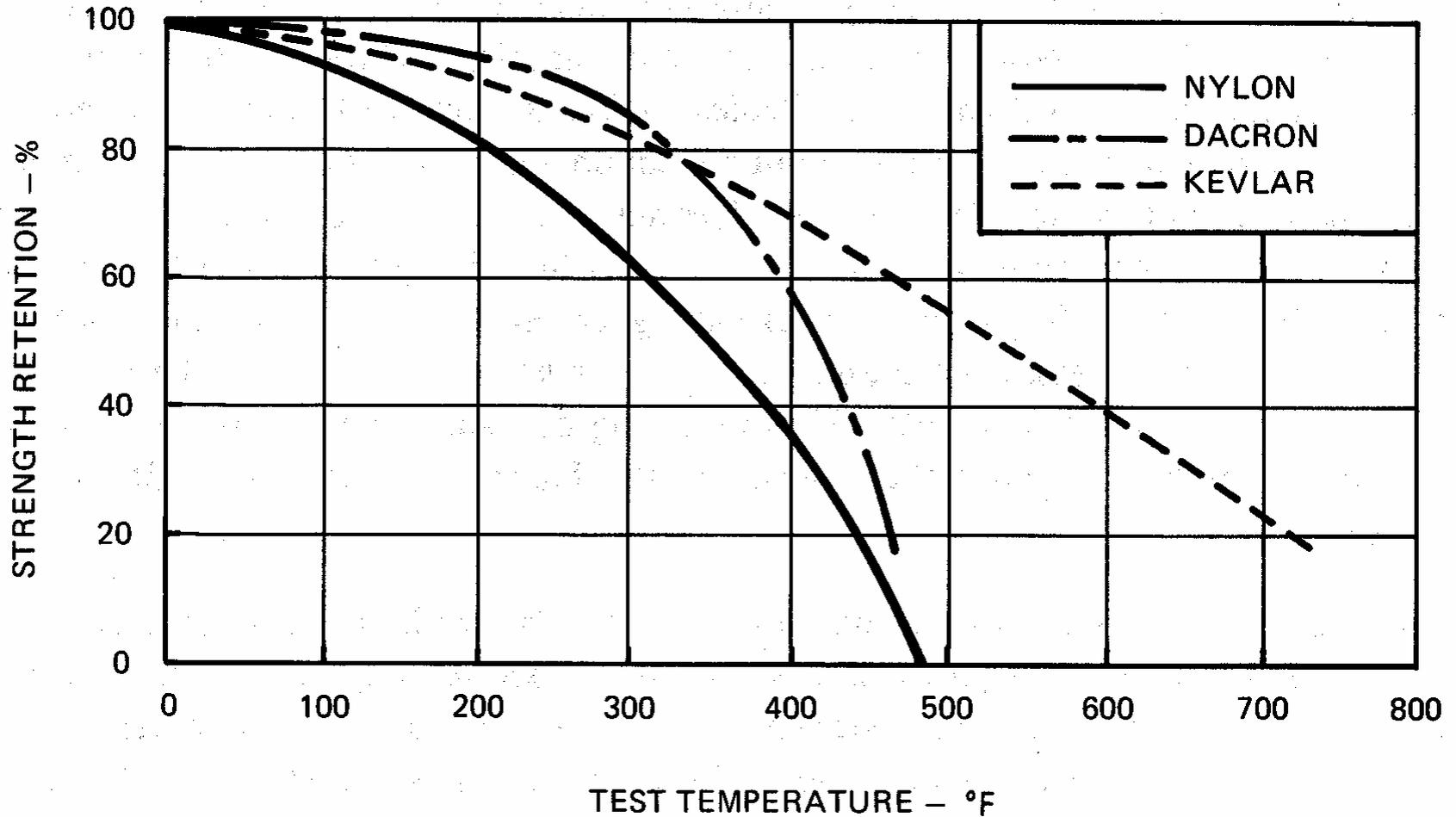
Effects of Light on Zylon



Comparison of Some Materials



Temperature Effects



Specifications

- **Military Specifications**
 - Have been deactivated but are still commonly used to specify materials in purchases
- **Commercial Specifications**
 - Supplier
 - National organizations (e.g. SAE, PIA)
- **Customer Specifications**
- **Detailed vs. Performance Specifications**
 - Suppliers prefer performance specs
 - Must make sure all necessary properties are specified in specifications

Specifications (continued)

- **Performance**

- Strength
- Weight
- Elongation
- Permeability
- UV resistance
- Allowable defects
- Color, etc.

- **Detailed**

- Threads per inch
- Weave pattern
- Yarn twist
- Width, etc.

See Knacke, Sections 6.6.3 and 6.6.5.3 for an extensive (but not exhaustive) list of material specifications

Products of Weaving

- **Broad-goods**
- **Narrow-goods**
- **Cord**

Broad-goods

- **Produced on looms**
 - Shuttle
 - Rapier
 - Water-and-air jet
- **Woven in 36-, 48-, 60-, and 72-inch widths and different weave patterns**
 - Plain
 - Twill
 - Taffeta
 - Satin
 - Ripstop
 - Selvage Edge

Finishing

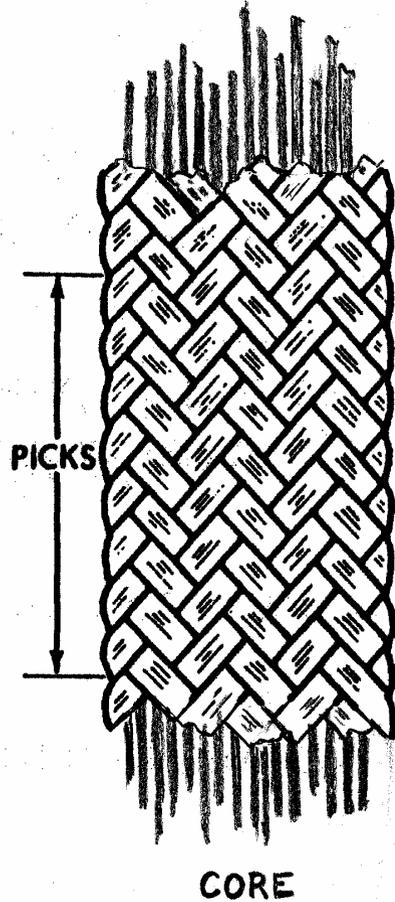
- **Greige goods**
- **Finishing processes(Converters)**
 - *Washing/Bleaching*
 - *Dyeing*
 - *Calendering*
 - *Coating*

Narrow Goods

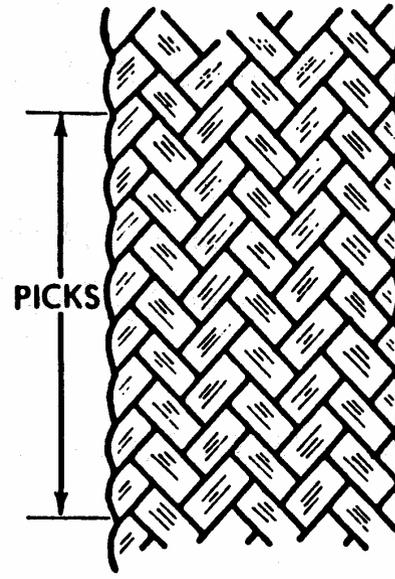
- **Usually less than 12 inches wide**
- **Weavers very skilled in developing new weaves**
 - Compromise between fiber translational efficiency and joint efficiency
- **Used in parachute systems for**
 - Suspension lines
 - Radials
 - Reinforcements
 - Risers
 - Bridles, etc.

Braided Cord

- With Core



- Coreless



Thread

- **Obviously used for sewing joints**
- **Twist can confound use in sewing machines**
- **Used to tie or tack textile components together for various reasons**
- **Many times waxed when used for tacking**
- **Generally use the same type thread material as being sewn (e.g. Kevlar in Kevlar, Nylon in Nylon)**
- **Nylon thread can melt in sewing machines if precautions are not taken**

Textile Drawings

- **Different than more common solid modeling drawings**
 - **Thickness depicted only by a single line for fabric, tapes, or webbing. (Cord can be shown as circular or elliptical in cross-section)**
 - **No cross hatching of textile components in “cutaway” views**
 - **Hidden edges not depicted**
 - **Dashed lines used to show stitching**
- **Defined in ANSI/AIAA-S-017-1991**

Outline

- Stress Analysis Methods
- Stress Analysis Code Examples
- Simplified Stress Analysis Examples

Parachute Stress Analysis Tools

- Simplified methods
- CANO code
- CALA code
- Commercial finite element codes

Simplified Methods

- Load carrying structure – suspension lines, radials or other reinforcements
 - **Estimated distribution of total load in parallel elements**
 - **Estimates based on geometry, shape from photographs, material stiffness**
- Pressurized structure – canopy
 - **Membrane theory – load/unit length = (K) (pressure) (radius of curvature)**
 - **K = 1.0 for cylinder**
 - **K = 0.5 for hemisphere**
 - **Radius of curvature from photograph or characteristic length**

CANO Code

- Developed by Northrop Ventura in 1960s
- Initial solutions used desk calculators
- Used for stress analysis of Apollo parachutes
- Many modifications now exist
- Good users manual written by University of Minnesota
- Version exists that includes verticals in ribbon parachutes
- Non-vertical solutions take seconds on modern PCs

CANO Code

- Early “finite element” code
- Original convergence algorithm not sophisticated
 - **May require patience**
- Modified algorithm developed by University of Minnesota
- Solutions starts at skirt and converges at vent
- Models parachute canopy gore
- Inputs
 - **Element geometry, parachute load, normalized pressure distribution, load/strain tables for materials**

CALA Code

- Developed at Sandia in the 1980s
- More modern numerical formulation than CANO
- Solution starts at vent and converges at skirt
- Models parachute canopy gore
- More general boundary conditions
 - **Pull-down vent**
 - **Attached pilot chute**
- More complicated input than CANO
- Input
 - **Element geometry, dynamic pressure, pressure coefficient distribution load/strain curves for materials**

Commercial Finite Element Codes

- Several commercial PC-based finite element software packages exist
- Specialized input/output formats for parachute stress analysis needed to make them user friendly for parachute engineers
- Potential for analysis of more general parachute canopy shapes and types of construction than CANO and CALA
- Potential for dynamic inflation modeling

Stress Analysis Examples

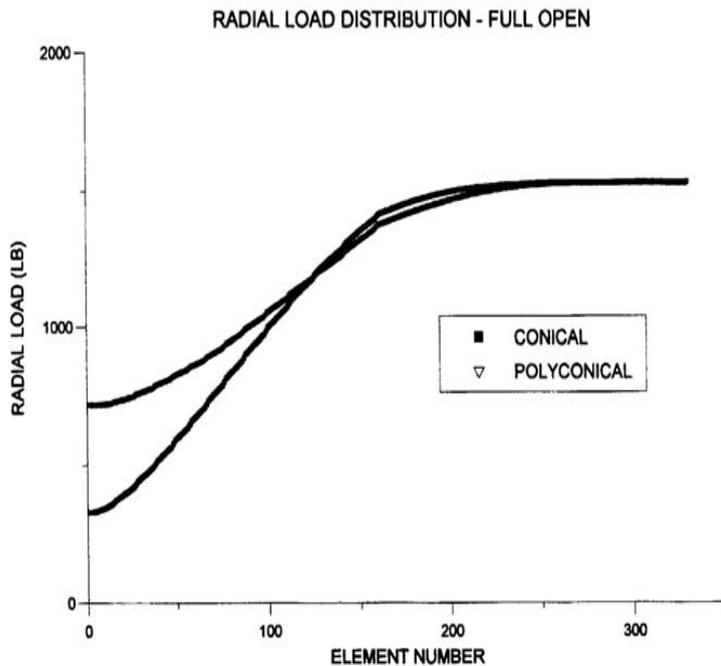
- SRB lightweight main parachute
- Space Shuttle Orbiter main parachute
- Space Shuttle Orbiter pilot parachute
- X-38 pilot parachute
- First stage floor panels for X-38 parafoil
- Fabric foam container

SRB Lightweight Main Parachute

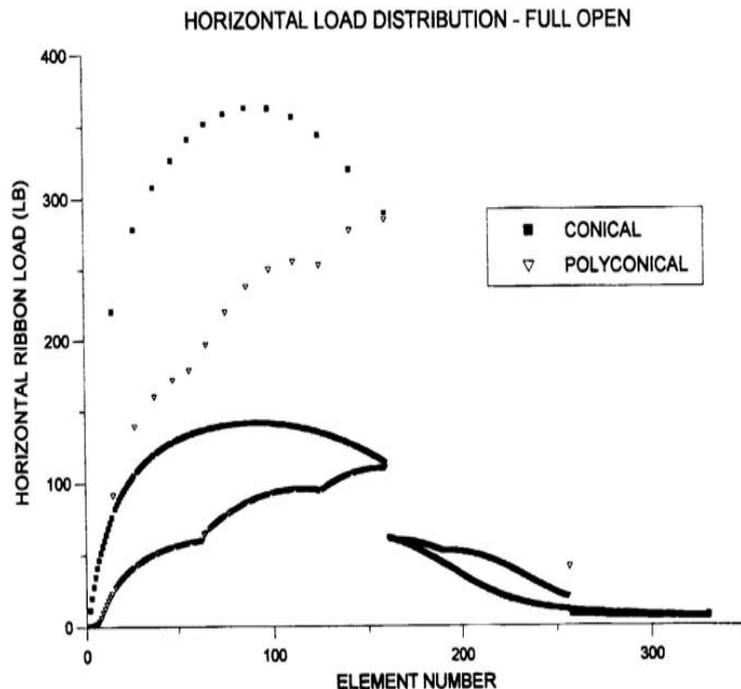
- **New main parachute designed to reduce weight and increase Shuttle payload**
 - Existing parachute weight = 2150 lb
 - New parachute weight = 850 lb
- **124-ft Kevlar/Nylon ribbon parachute with solid cloth material near the skirt**
- **Design load increased from 175,000 lb to 210,000 lb**
- **Canopy design was polyconical (5 section) approximation to a quarter spherical shape**
 - **Primarily to reduce canopy loads and reduce material weight**

SRB Lightweight Main Parachute

- CANO analysis used to support decision to use polyconical design
- Comparison with traditional 20 degree conical design
- Loads in primary load carrying structure were shown to be similar for both designs

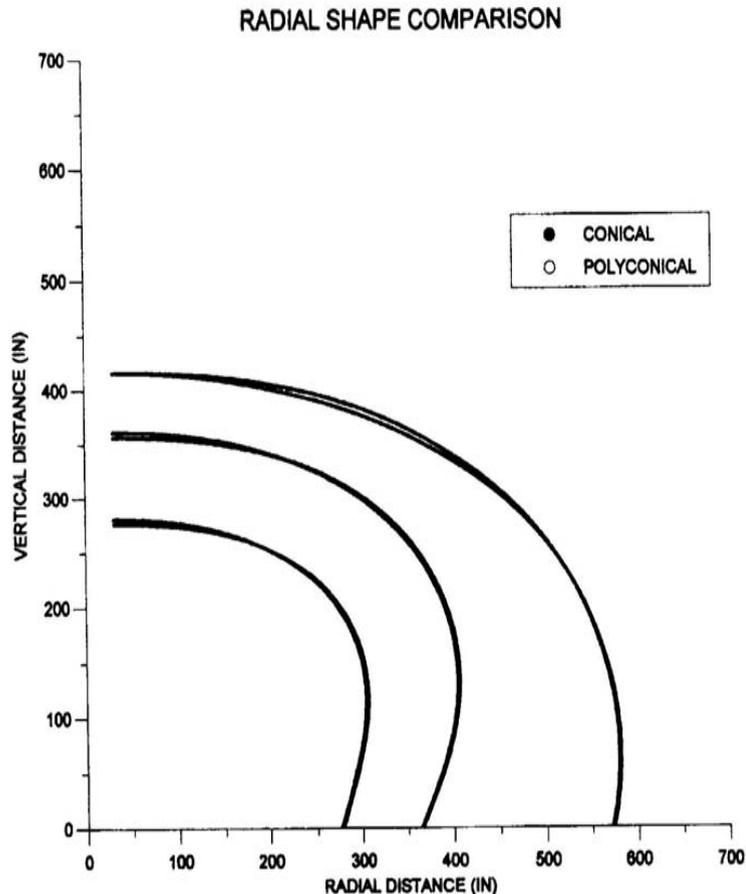


SRB Lightweight Main Parachute



- Horizontal ribbon loads were shown to be significantly lower for the polyconical design
 - **Higher points are for ripstops**
 - **Lower curves are for ribbons and fabric**
- Lower loads allowed use of lighter materials

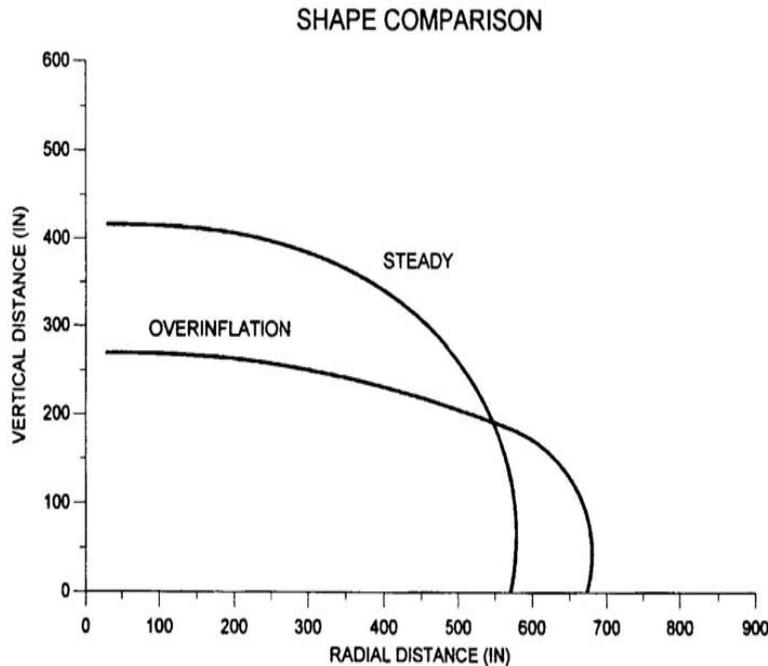
SRB Lightweight Main Parachute



- CANO results were also used to show that inflated shapes would not be much different than for conical canopy
 - **Conical canopy performance experience would still be valid**
 - **Reefing data for conical canopies could be used**

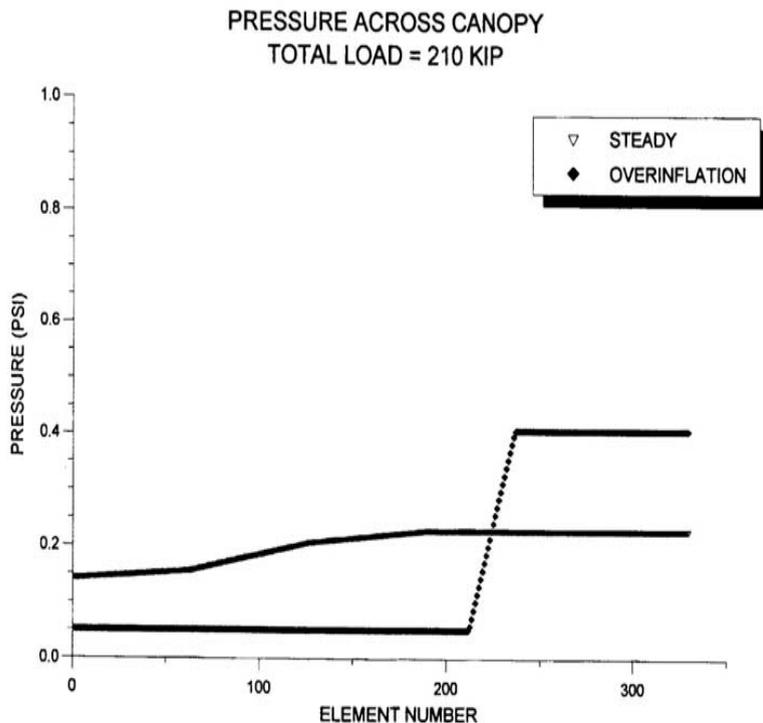
SRB Lightweight Main Parachute

- 1st test showed some fabric failures near the skirt during canopy overinflation
- CANO results were used to study the fabric loads in an overinflated canopy



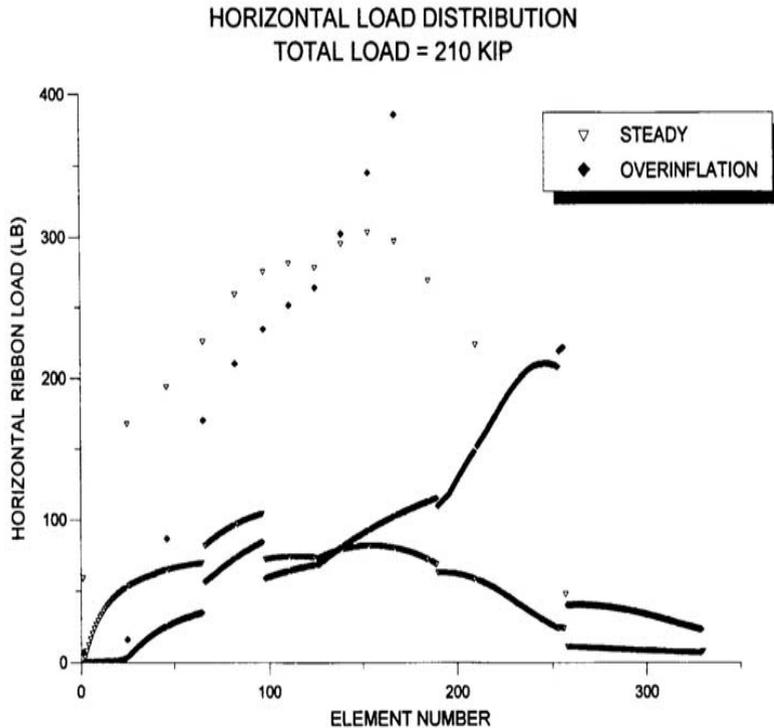
SRB Lightweight Main Parachute

- A pressure distribution was derived that produced the same CANO shape as that observed during the 1st test

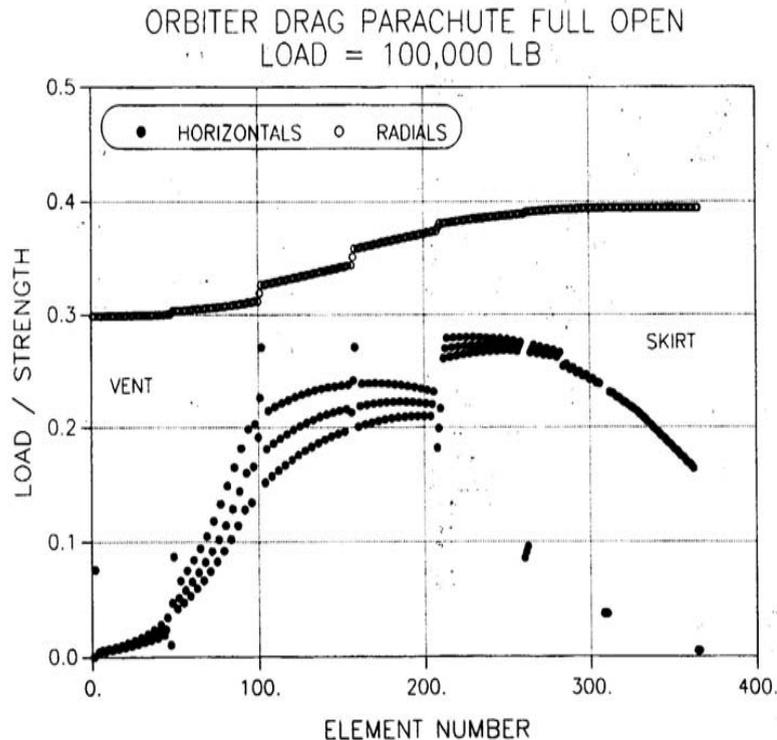


SRB Lightweight Main Parachute

- CANO loads for the overinflated shape were not sufficient to cause failure of undamaged fabric
- The very lightweight fabric near the canopy skirt was being damaged during deployment at the high SRB bag strip velocities



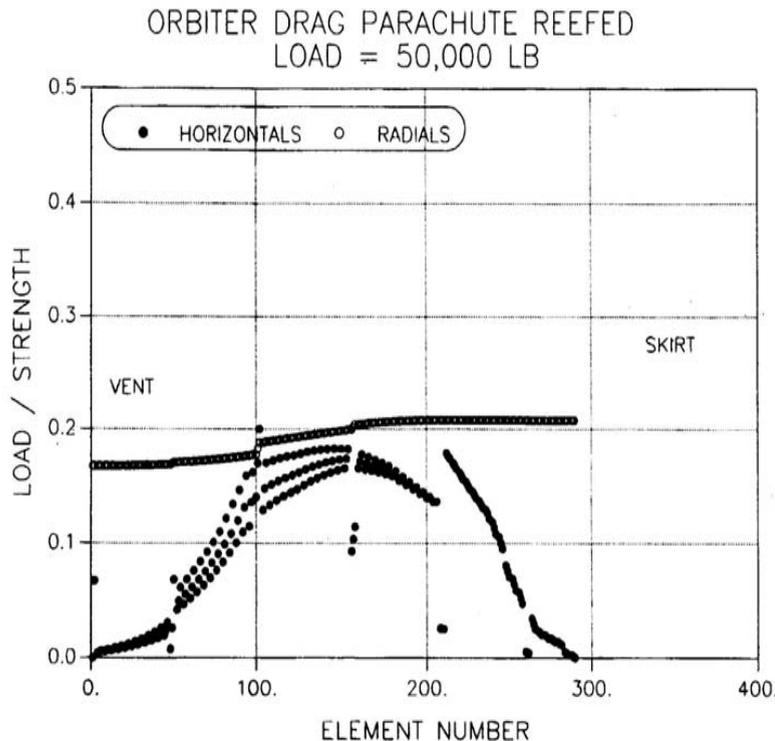
Orbiter Drag Parachute



- Decision to reuse the Orbiter drag parachute required detailed loads analysis
- A CANO analysis provided the loads data necessary for inspection and repair work at the KSC PRF

Orbiter Drag Parachute

- Load/strength ratio provides the inverse of available design factor in structure
- Parachute was originally designed without reefing so reefed loads are low



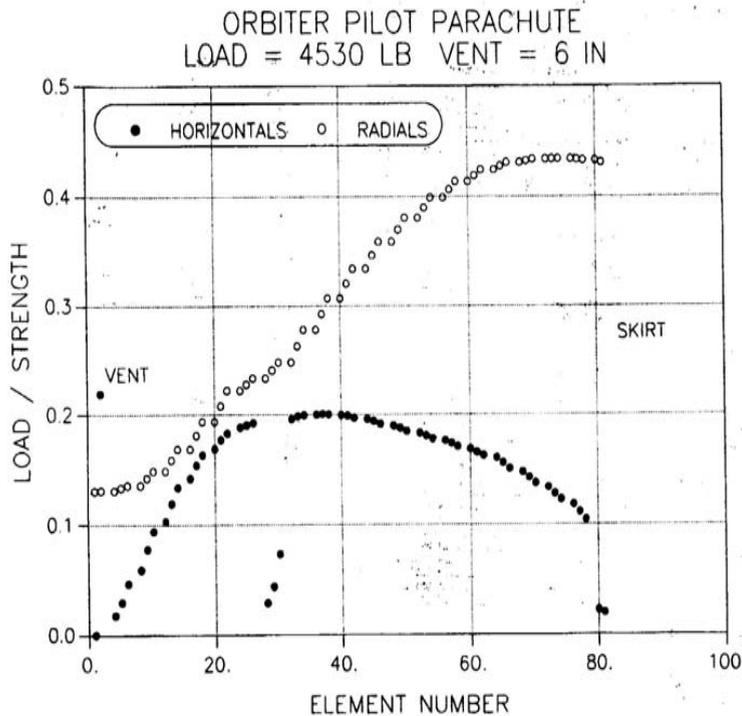
Orbiter Drag Parachute

Comparison of Ribbon Load Estimates

- Full Open Design Load $F = 100,000$ lb and Projected Area $A = 628$ ft²
- Average Pressure $p = F/A = 159$ lb/ft²
- Hoop Tension Formulas
 - $T/\ell = (\delta p) R$ for cylinder
 - $T/\ell = (\delta p) R / 2$ hemisphere
- From CANO Analysis Maximum $T/\ell = 38$ lb/in
- For Hemisphere $T/\ell = 93$ lb/in - Too High
- For Cylinder With $R =$ Gore Width, $T/\ell = 40$ lb/in

Orbiter Pilot Parachute

- Decision to reuse the Orbiter pilot parachute also required CANO loads analysis to support inspection and repair
- Radial strength not robust

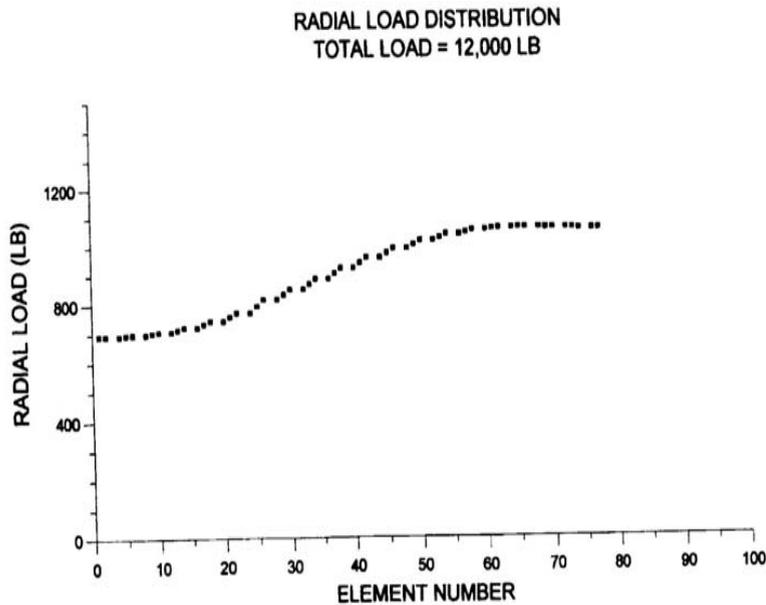


X-38 Pilot Parachute

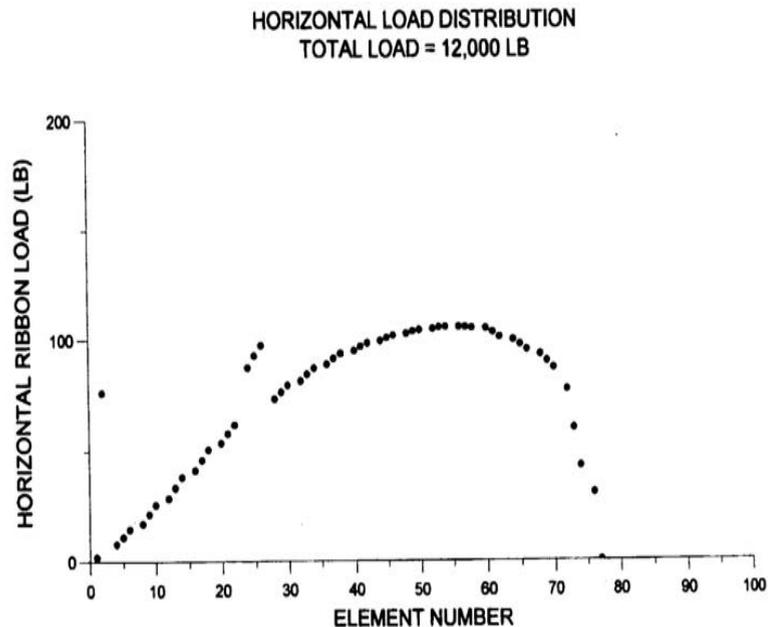
- X-38 Project wanted to use Orbiter mortar and pilot chute to reduce development costs
- A much higher design load was required for the pilot parachute
 - **12,000 lb for X-38**
 - **4500 lb for Orbiter**
- Kevlar suspension line and radial overlay was added to the existing canopy to provide the required strength
- Total weight was slightly less than all Nylon chute

X-38 Pilot Parachute

- Radial load distribution in modified Orbiter pilot parachute
- Required strength in Kevlar load carrying structure



X-38 Pilot Parachute



- Horizontal load distribution in modified Orbiter pilot parachute
- Adequate strength in existing horizontals
- Stiff radial structure keeps loads in horizontals low

X-38 Parafoil First Stage Floor Panel

- During the X-38 parachute development program, a “zero” reefed stage was tried to promote inflation symmetry in the first reefed stage
 - **The “zero” stage reefing was suspension line reefing that pulled the parafoil corners down into a semi-round configuration**
- Unfortunately, disreef from the “zero” stage was very rapid and dynamic
 - **A parafoil floor failure occurred**
 - **The very large radius shape at failure suggested a membrane stress calculation**

X-38 Parafoil First Stage Floor Panel

- Hoop Tension $T/\ell = (\delta p) R$
 - δp = pressure across fabric
 - R = radius of curvature
- Unsteady Pressure $\delta p = \delta C_p C_k Q$
 - δC_p = steady pressure coefficient across fabric
 - C_k = shock factor
 - Q = dynamic pressure
- Estimate $\delta p = (1.2)(2)(10 \text{ lb/ft}^2) = 24 \text{ lb/ft}^2 = 0.17 \text{ lb/in}^2$
- Maximum Radius = Suspension Line Length = 767 in
- Hoop Tension $T/\ell = (0.17 \text{ lb/in}^2)(767 \text{ in}) = 130 \text{ lb/in}$

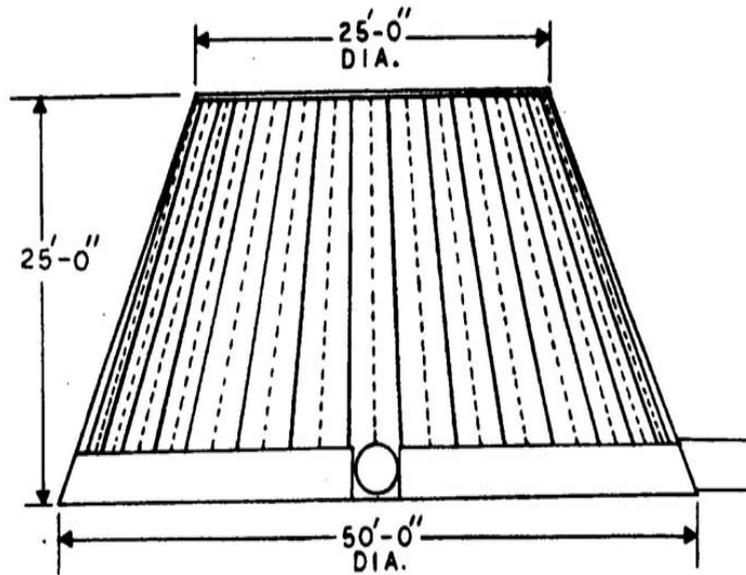
X-38 Parafoil First Stage Floor Panel

- Floor Panel Fabric Strength was $T/\ell = 100 \text{ lb/in}$ so Decision was Made to Increase Fabric Strength
- Under Steady State Conditions the Radius of Curvature was Proportional to the Cell Width Because All Suspension Lines Were Loaded
- Maximum Radius = 3 Times Cell Width = 144 in
- Hoop Tension $T/\ell = (0.17 \text{ lb/in}^2)(144 \text{ in}) = 25 \text{ lb/in}$
- Original Design was Adequate Under Steady State Conditions

Fabric Foam Containers

- Aqueous foam has been used as an effective medium for the mitigation of explosive effects
- Lightweight portable fabric structures were developed to contain the aqueous foam around the explosive charge
- Several different containment structures were developed and tested under realistic deployment conditions
- Containers were designed to hydrostatic pressure using membrane equation

50-ft Conical Container



- Sketch with dimensions of 50-ft conical container

50-ft Conical Container



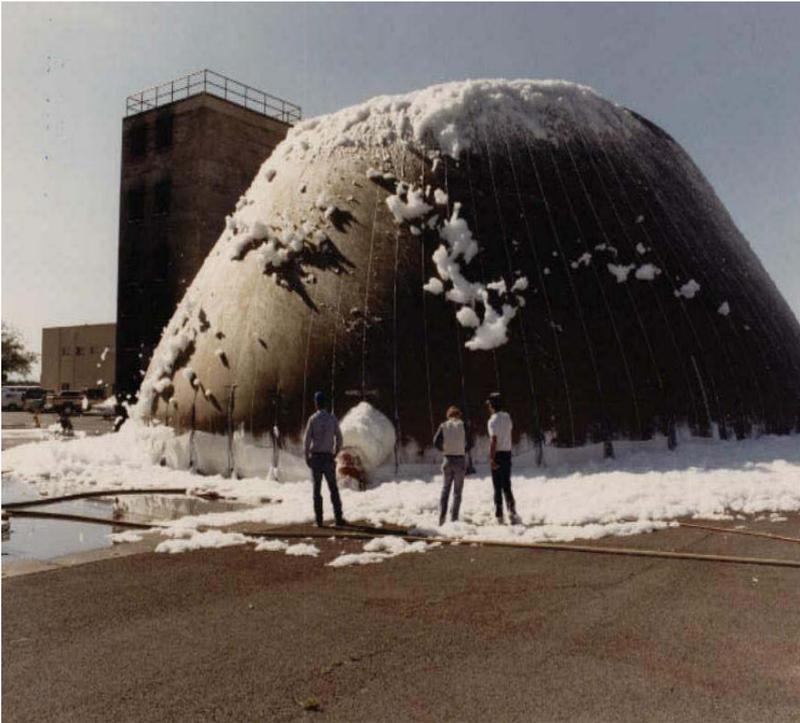
- 50-ft conical container filled
- Conical containers were filled from top

50-ft Conical Container



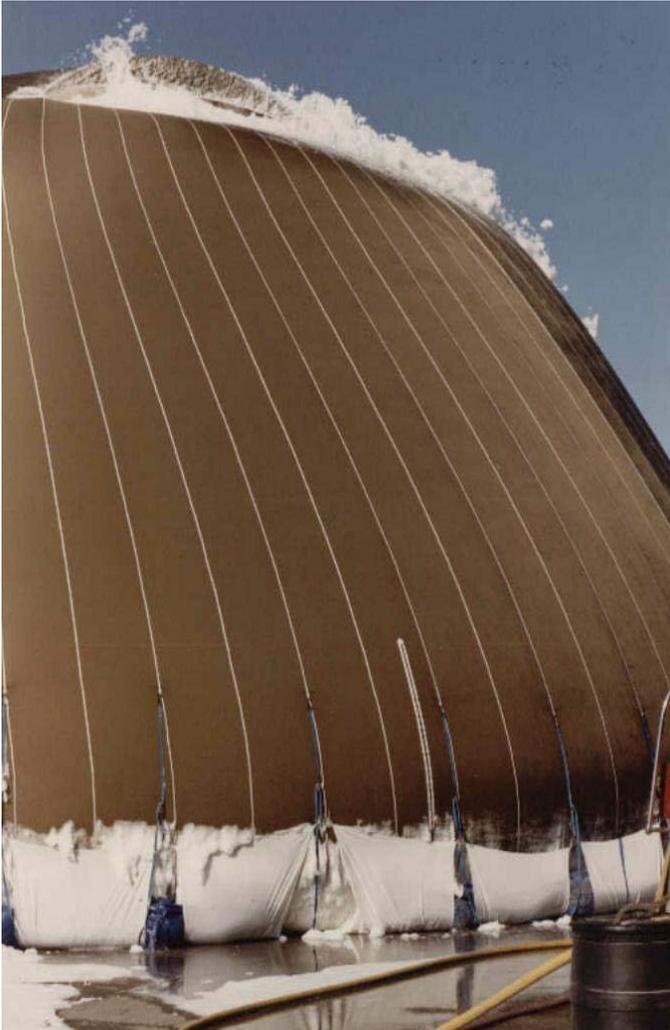
- 50-ft conical container personnel access opening
- Access openings were closed with heavy duty zippers

70-ft Conical Container



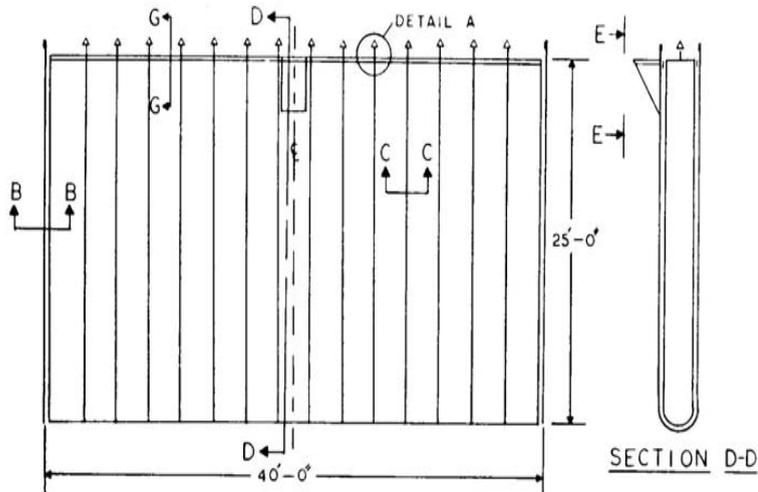
- 70-ft conical container filled
- Container deliberately overfilled to test structure

70-ft Conical Container



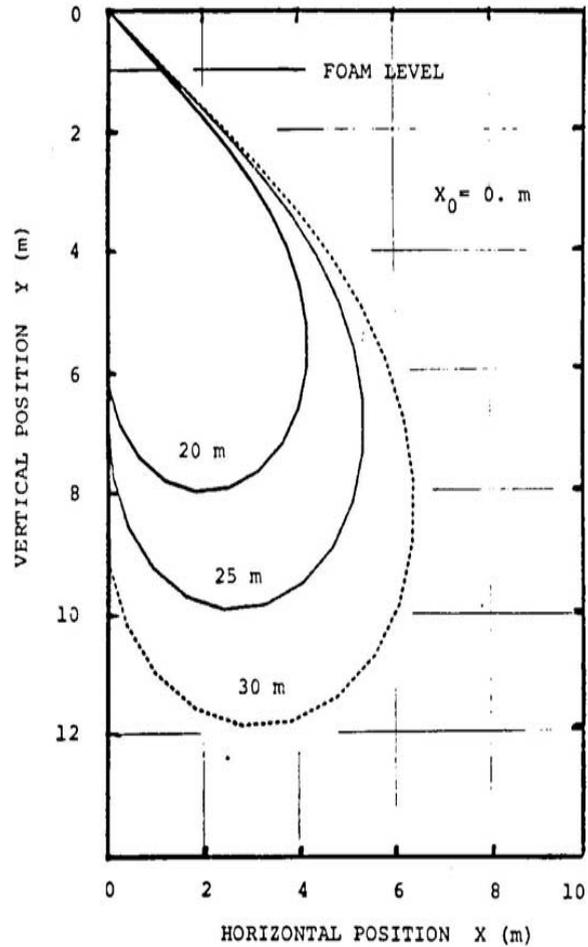
- Close up of 70-ft conical container filled
- Personnel access opening zipper at base in center

Vertical Wall Container



- Sketch with dimensions of vertical wall container

Vertical Wall Container



- Predicted shapes of different sized vertical wall containers
- Membrane theory use to predict shape





Vertical Wall Container



- Vertical wall container filled
- Vertical wall container filled from top