

# Thermal Engineering for the Beagle 2 Mars Lander Surface Operations

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# Acknowledgment

- Dr Simon Peskett, who preceded me as lead thermal engineer on Beagle 2 until he left RAL at the end of 2001.

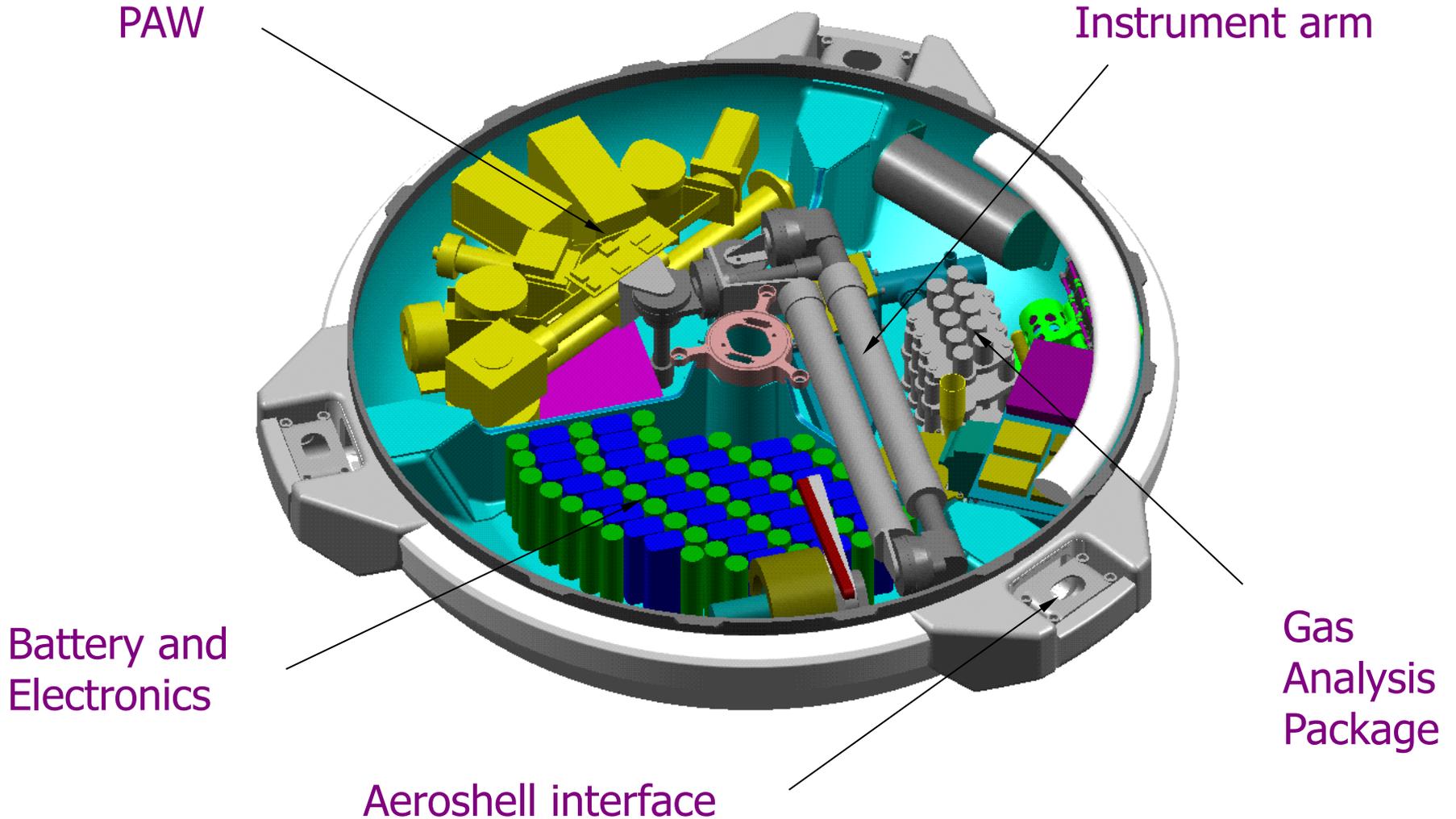
# Mission Overview

- Launched June 2003 aboard ESA's Mars Express – to look specifically for signs of life. Seven month Cruise, followed by five day Coast (no telemetry available)
- Landing site in the Isidis Basin ( $11^{\circ}\text{N}$   $90^{\circ}\text{E}$ )
- Early spring northern hemisphere ( $L_s = 322^{\circ}$ ). Baseline mission of 180 Sols (to  $L_s = 60^{\circ}$ )
- Landing planned for Christmas morning 2003 but no communication achieved with Beagle 2



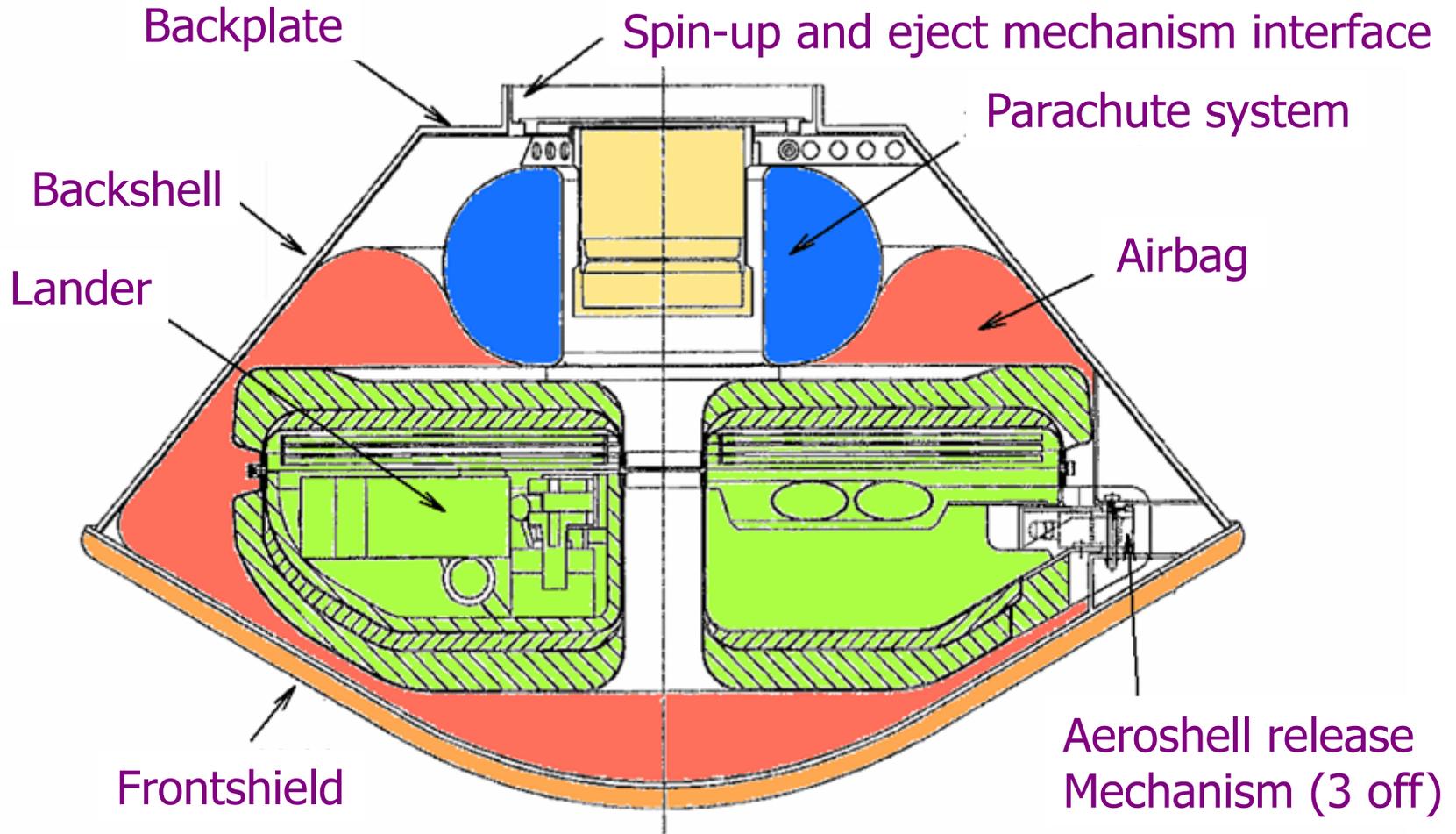
Lander model on the NASA Johnson Space  
Centre Mars Simulation Surface

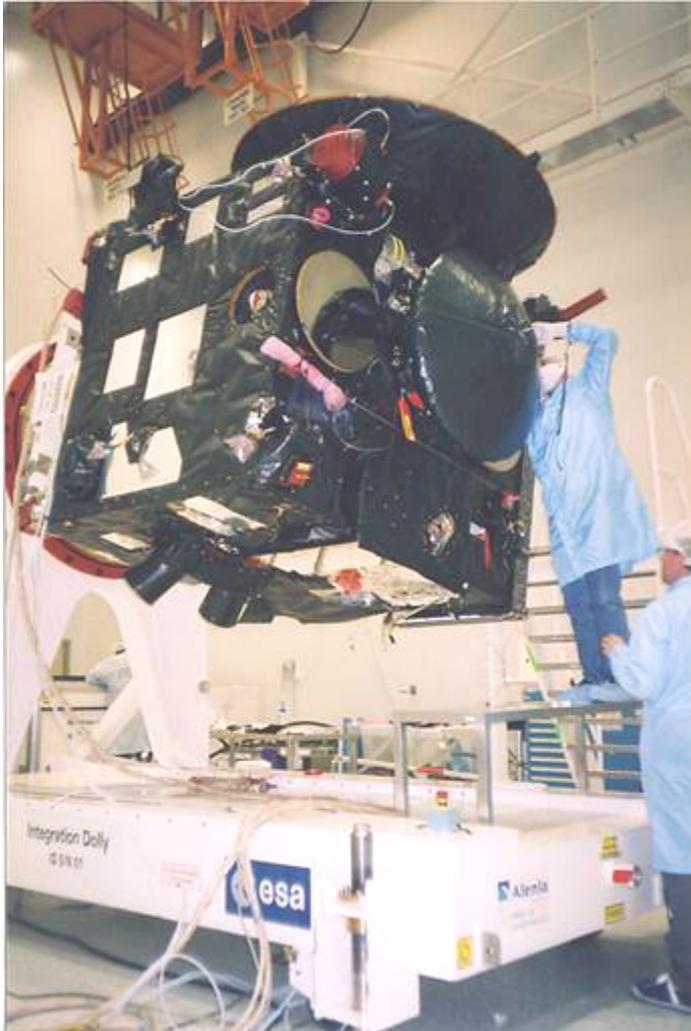
# Inside the Lander



- Beagle 2 was packed like a tourist's suitcase!
- Examine soil, rocks, and atmosphere for evidence of life
  - Instrument arm
  - Beagle's 'PAW' and the 'Mole'
  - Gas Analysis Package
- Martian weather reports
- Age, chemistry, and composition of the Mars surface
- Cameras

# Journey to Mars - the Probe

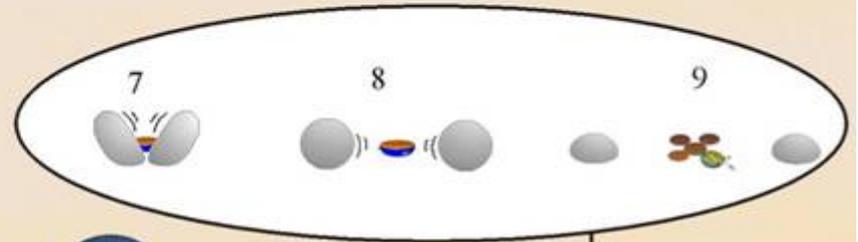




Integration of Beagle 2  
multi-layer insulation at  
the Baikonur Cosmodrome

# Landing Sequence

## Mars Express Beagle 2 - Entry, Descent & Landing System

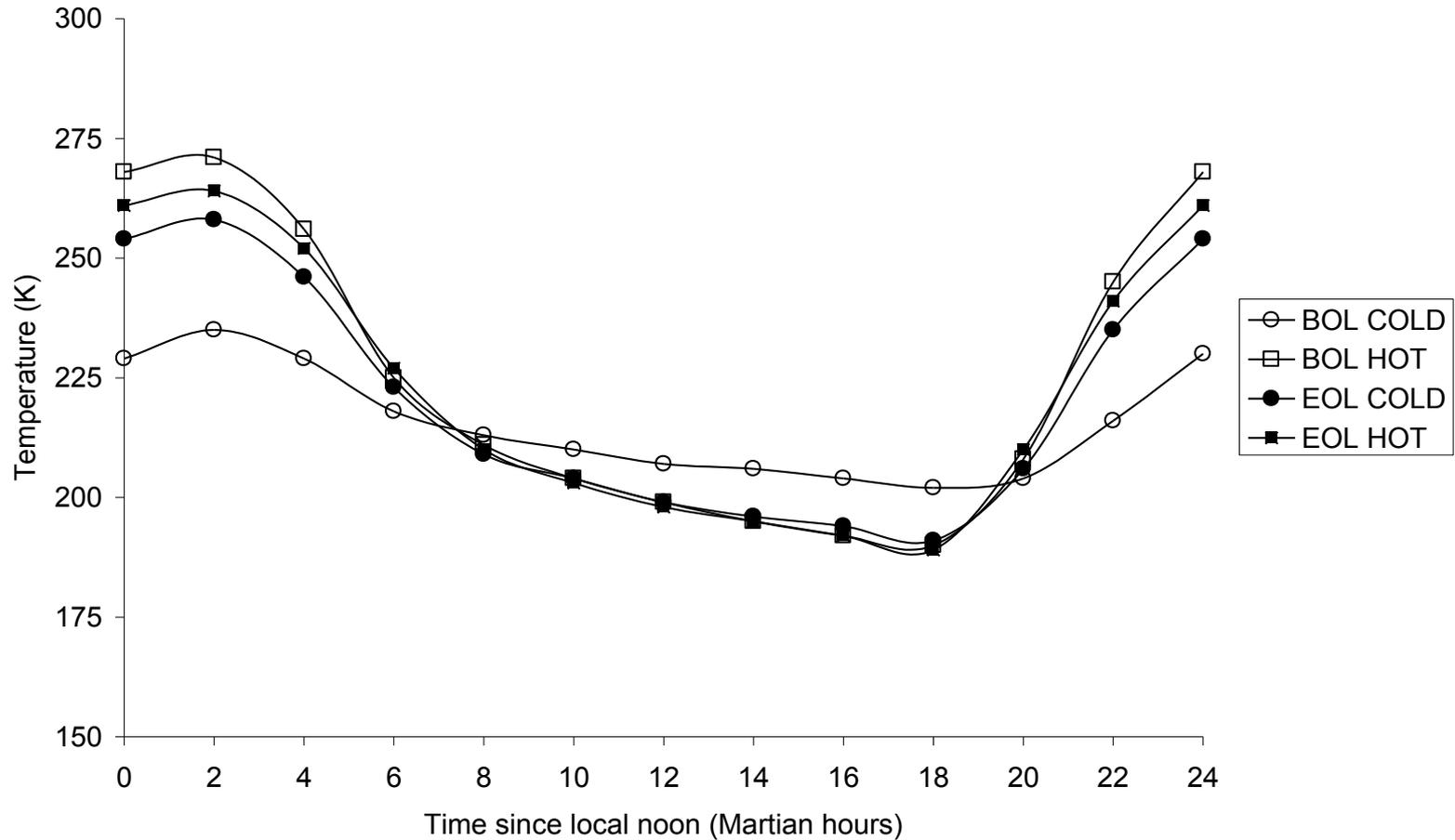


- 1 - Entry into Mars atmosphere. 0 s, 124 km, Mach 31.5.
- 2 - Pilot chute deployment. 117 s, 7.8 km, Mach 1.5.
- 3 - Back cover release and main chute deployment. 152 s, 4.2 km, Mach 0.44.
- 4 - Heat Shield separation. 155 s.
- 5 - Airbag inflation.
- 6 - Touchdown and riser cut. 281 s.
- 7 - Airbag separation. Landing + 5 mins.
- 8 - Lander righting and deployment. Landing + 6 mins.
- 9 - Lander deployed. Landing + 10 mins.

- Direct and diffuse solar radiation
- Radiative losses to effective sky temperature
- Radiative and conductive losses to surface
- Convective losses to local environment

- Environmental conditions influenced by the level of dust (optical depth) in the atmosphere.
- Time of landing ( $L_s = 322^\circ$ ) shortly after the dust storm season. Optical depths:
  - Can exceed 5.0 during dust storm
  - 1.0 measured by Viking, decreasing to 0.5 through spring and summer
  - 0.2 measured by Mars Global Surveyor
- Surface temperatures:  $\sim 0^\circ\text{C}$  early afternoon to  $\sim -100^\circ\text{C}$  just before dawn
- Sky temperature:  $-100^\circ\text{C}$  to  $-150^\circ\text{C}$
- Wind speeds typically less than 10 m/s

	<b>COLD</b>		<b>HOT</b>	
<b>PARAMETER</b>	<b>BOL</b>	<b>EOL</b>	<b>BOL</b>	<b>EOL</b>
Aerocentric longitude (°)	322	60	322	60
Latitude (°)	31	31	0	0
Optical depth (-)	2.0	0.7	0.2	0.2
Wind speed (m/s)	10	10	0	0
Interface with surface	'raise d'	'raise d'	'fir m'	'fir m'
Dust coverage (%)	-	100	-	24



Assumed surface temperatures  
(taken from Mars Climate Database)

# Requirements

- Minimize energy required by survival and operational heaters
- Maintain temperatures within applicable limits:

UNIT	NON-OPERATIONAL (°C)		OPERATIONAL (°C)	
	MIN	MAX	MIN	MAX
Battery	-	-	-30	45
Common electronics	-	-	-50	55
Transceiver	-65	55	-65	55
Gas Analysis Package	-65	40	-40	30
Instrument arm	-100	125	-60	30
Solar arrays	-120	-	-	40

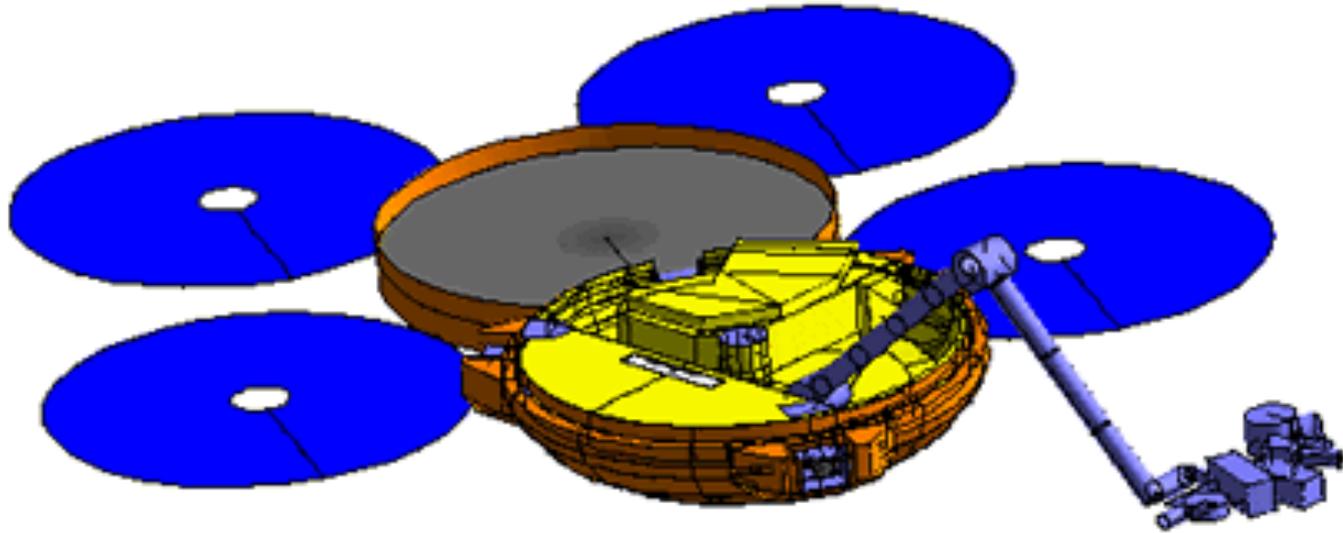
- Thermally isolate battery from structure (low conductance mounts; radiative shielding)
- Thermally couple electronics to battery ( $\sim 8\text{W}$  stand-by dissipation)
- Foam insulation
- Low-emissivity finishes
- Use of survival heaters on battery and elsewhere where necessary
- Qualify components to accommodate wide temperature fluctuations

- Two approaches were considered for keeping battery warm:
  - Radioisotope heater unit (RHU) coupled to battery
    - 8.5 W dissipation
  - A solar absorber unit (SAU) architecture to optimize absorption of incident solar radiation together with a phase change material (PCM):
    - Tinox solar absorber ( $\alpha_s > 0.94$ ,  $\varepsilon < 0.05$ )
    - 1.5 kg water PCM

- Conclusions of trade-off:
  - Both approaches feasible for Lander thermal design
  - RHU approach less sensitive to variations in Lander design parameters, but had narrow design margins in some areas
  - Other technical difficulties with RHUs (e.g., heat rejection system during Cruise/Coast)
  - Conclusion was to focus on development of the SAU approach

- The use of different solar absorber materials and PCM options was considered.
- Solar absorber materials:
  - Tinox ( $\alpha_s > 0.94$ ,  $\varepsilon < 0.05$ )
  - Germanium x VDA x Kapton ( $\alpha_s \sim 0.6$ ,  $\varepsilon \sim 0.05$ )
  - Hybrid Tinox/Germanium
- PCM options:
  - None
  - 0.5 kg and 0.86 kg water
  - 0.5 kg and 0.77 kg dodecane wax (melting point  $\sim -10$  °C)

- Under cold conditions water PCM could stay frozen
- A 0.77 kg dodecane PCM had improved response compared with 0.5 kg water, but increased mass was a major concern
- 0.5 kg dodecane PCM was marginal at BOL cold conditions
- Electronics may exceed upper temperatures in hot cases if high-absorptivity (Tinox) absorber used
- A Germanium x VDA x Kapton SAU architecture without a PCM was initially baselined



# Detailed Thermal Design

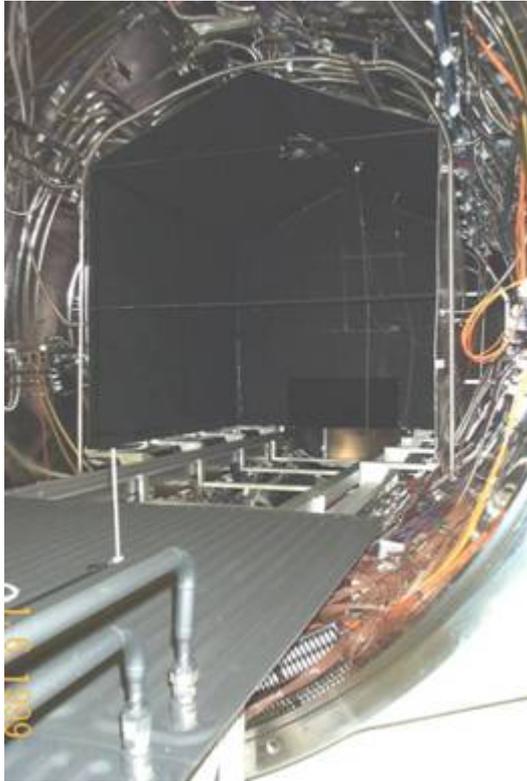
- Low conductance structure (glass-fiber reinforced plastic instead of aluminium honeycomb).
- Inner and outer surfaces of Lander structure gold coated
- Solar absorber finish now gold coated kapton
- Instrument arm wrapped in aluminized tape
- Software controlled heaters on battery, transceiver, and a small number of locations in Lander.

# Solar Absorber Unit

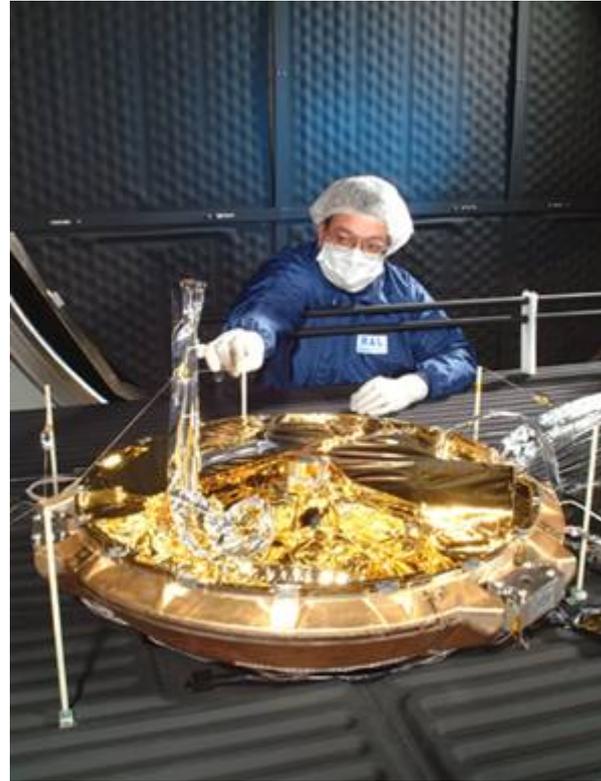


All Rights Reserved Beagle 2





Lander test  
shroud



Lander test  
model,  
RAL, May 2002

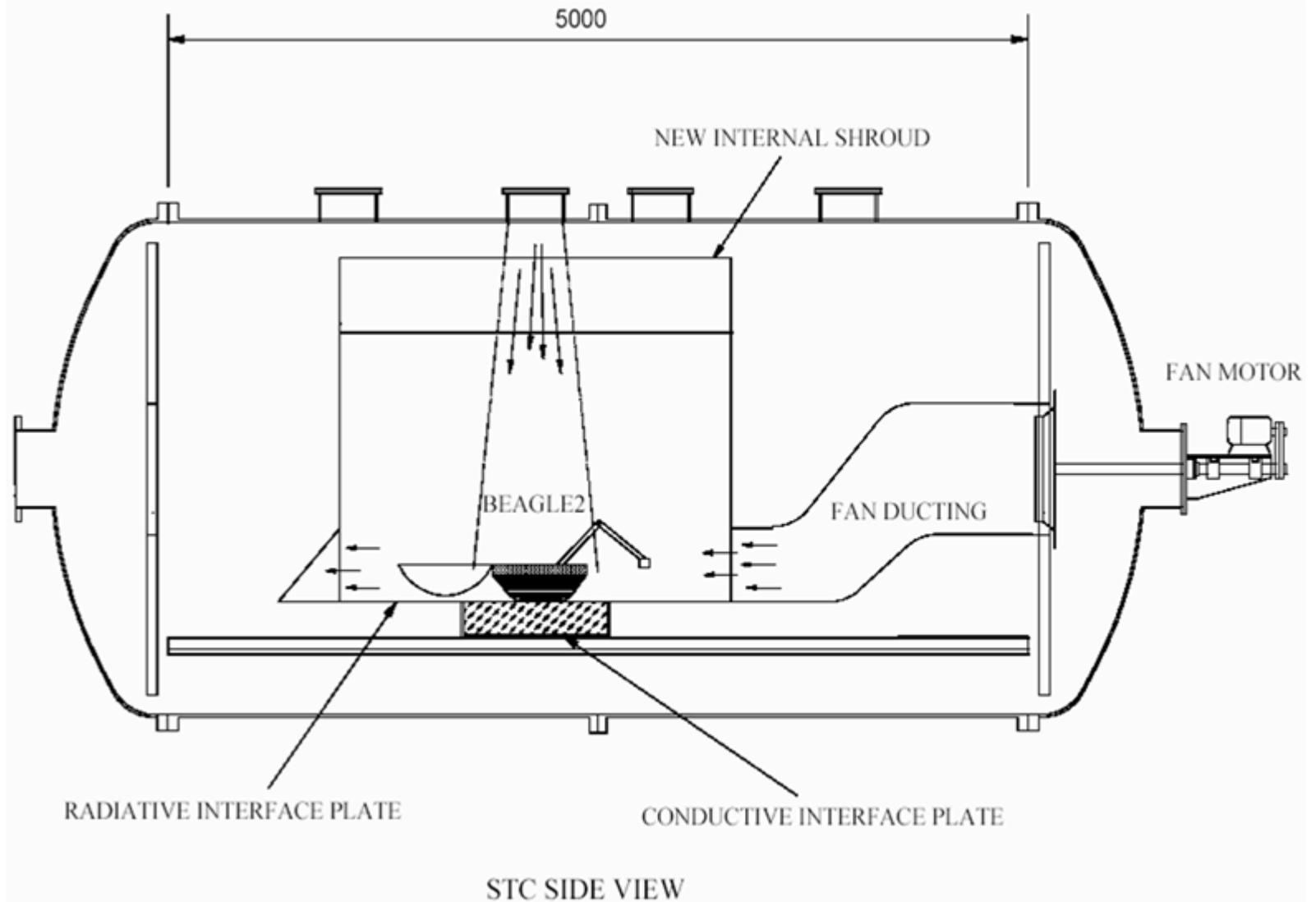


Probe test model,  
RAL, September  
2002

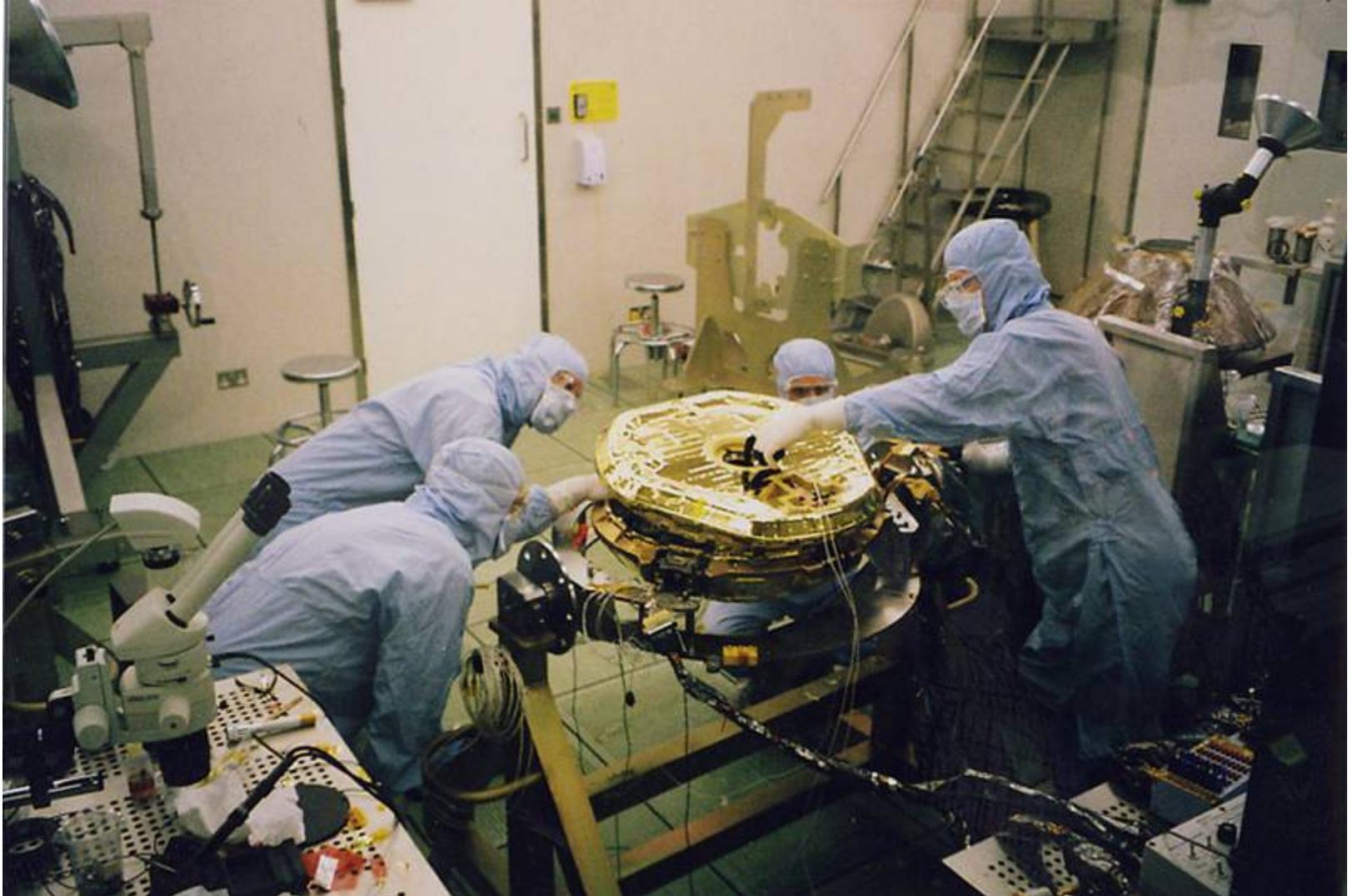
# Lander Test Requirements

	<i>Ideal</i>	<i>Specified</i>
<i>Lander Model</i>	<ul style="list-style-type: none"> <li>• Complete</li> </ul>	<ul style="list-style-type: none"> <li>• With lid, but no solar arrays</li> <li>• Partial instrument arm</li> </ul>
<i>Surface</i>	<ul style="list-style-type: none"> <li>• Sandy/rocky – like landing site</li> <li>• Temperature cycling between -100 and 0 °C</li> </ul>	<ul style="list-style-type: none"> <li>• Temperature controlled panels:               <ul style="list-style-type: none"> <li>◦ Beneath Lander</li> <li>◦ Surrounding Martian surface</li> </ul> </li> </ul>
<i>Atmosphere</i>	<ul style="list-style-type: none"> <li>• ~ 7 mbar CO<sub>2</sub></li> <li>• Temperature cycling between -100 and 0 °C</li> <li>• Winds up to 10 m/s</li> </ul>	<ul style="list-style-type: none"> <li>• ~ 7 mbar CO<sub>2</sub></li> <li>• Temperature not controlled</li> <li>• Winds up to 10 m/s</li> </ul>
<i>Sky-view</i>	<ul style="list-style-type: none"> <li>• -135 °C</li> </ul>	<ul style="list-style-type: none"> <li>• -100 °C</li> </ul>
<i>Solar simulator</i>	<ul style="list-style-type: none"> <li>• Moving beam</li> <li>• 0 – 600 W/m<sup>2</sup> intensity</li> </ul>	<ul style="list-style-type: none"> <li>• Vertically fixed beam</li> <li>• 0 – 600 W/m<sup>2</sup> intensity</li> </ul>

# Lander Test Implementation



# Closing Flight Model Lander



- Thermal design for the Martian environment is a great challenge
- A thermal design approach which did not require the use of RHUs was developed for Beagle 2
- The thermal design was verified by extensive testing at RAL

# Is there life on Mars?

