



MEDLI Aerothermal Environment Reconstruction Efforts

Todd White*, Ioana Cozmuta*, Jose Santos+, Bernard Laub
NASA Ames Research Center

Milad Mahzari
Georgia Tech

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Overview

- Description of MEDLI & MISP
- MISP Science Goals
- Aerothermal Reconstruction
- Material Properties and Modeling
- Sensor Modeling
- Predictor-Correctors
- Conclusions & Forward Work
- Acknowledgements



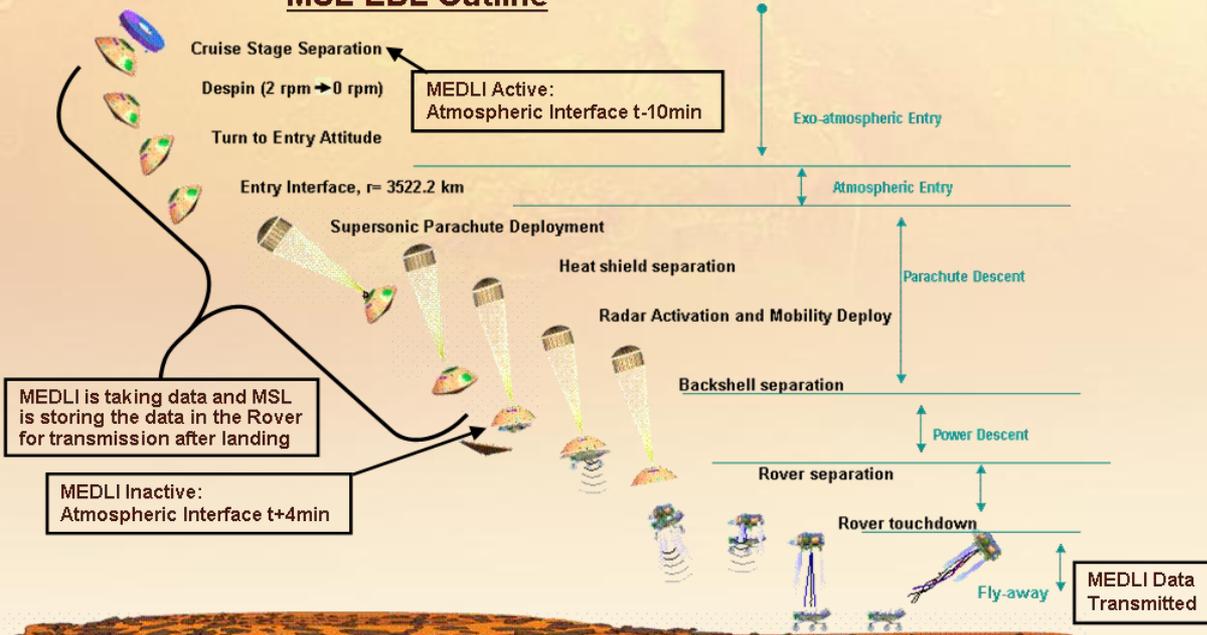


MSL Entry Descent and Landing Instrumentation (MEDLI)

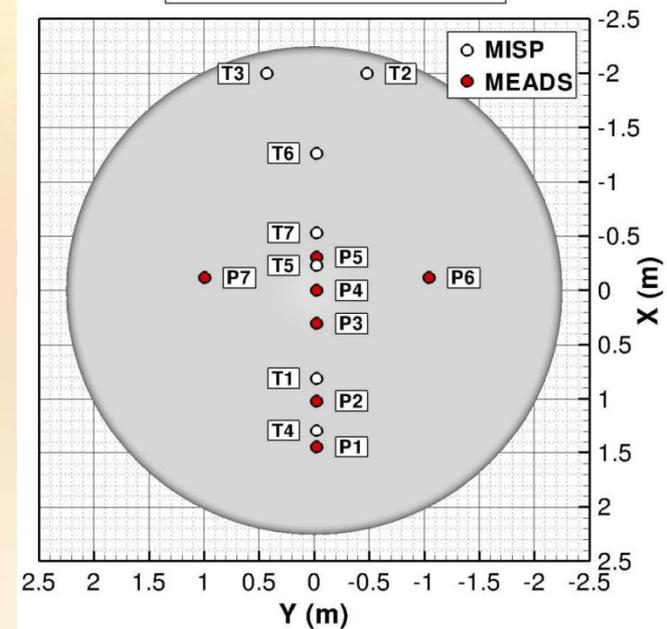
- Mars Science Laboratory (MSL) has a 4.5m diameter PICA tiled heatshield. It launches November 2011, and will enter Mars in the summer of 2012
- The heatshield is instrumented via MEDLI, with two main components
 - MEADS (Mars Entry Atmospheric Data System) Pressure ports and transducers, at 7 locations
 - MISP (Mars Integrated Sensor Plug)
In-depth sensors at 7 locations, embedded in TPS.



MSL EDL Outline



MEDLI Sensor Locations

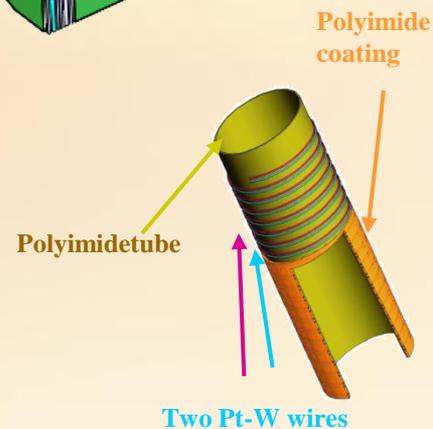
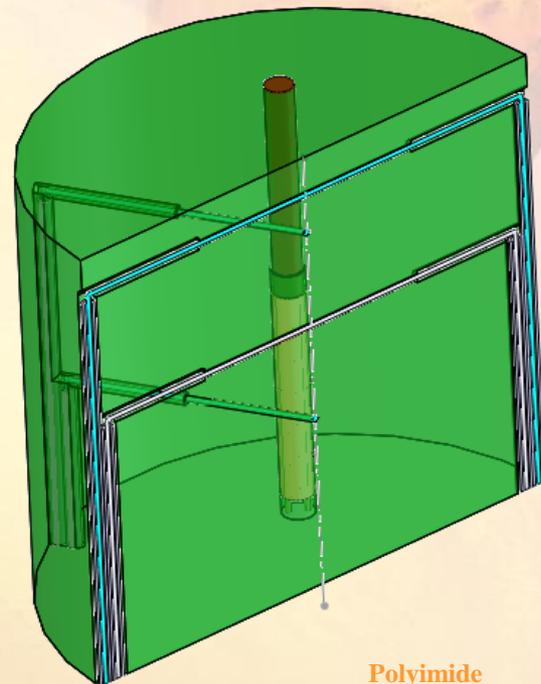




MISP (MEDLI Instrumented Sensor Plug)

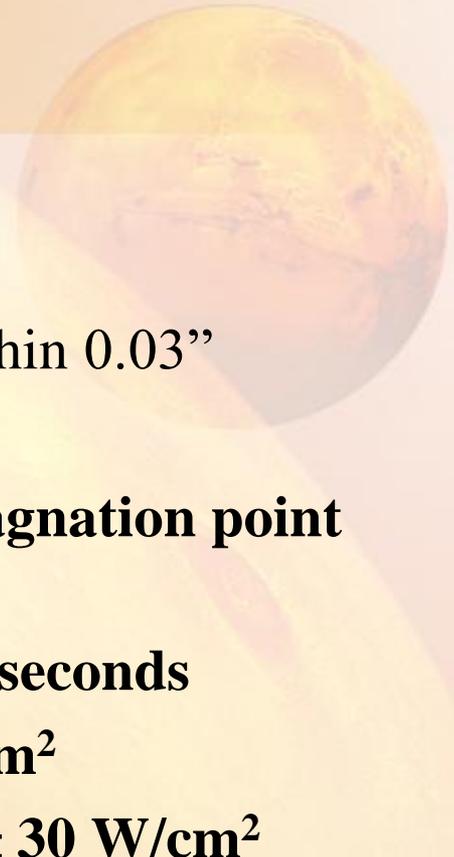
- Each MISP consists of four thermocouples in 1.1” diameter by 1.25” deep PICA cylinder, with
- **Four type-K thermocouples (TCs)** with range to 1300K:
 - Two near surface thermocouples (0.1” and 0.2”) are sampled at 8 Hz,
 - Two deeper TCs (0.45” and 0.7”) are sampled at 1 Hz.
- **One HEAT** (Hollow aErothermal Ablation and Temperature) sensor:
 - Wound Tungsten wires in Kapton tubing that is electrically conductive when charred, and changes resistivity (sampled at 8 Hz),
 - Often called a “Recession Sensor”, it does not measure recession, but tracks an iso-therm (720 deg C) through the material. For constant developed steady-state ablation, corresponds to recession rate.

Cross section of single MISP





MISP Science Goals

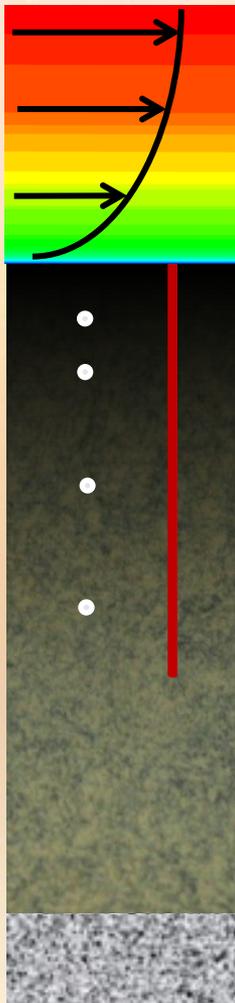


- MISP Requirements specifically call for:
 - Measure subsurface temperature within $\pm 12\%$
 - Track 720C iso-therm progression through TPS within 0.03”
 - **Determine total TPS recession within ± 0.25 ”**
 - **Reconstruct Basic distribution of heating and stagnation point heating within $\pm 30 \text{ W/cm}^2$**
 - **Determine time of turbulent transition, within 2 seconds**
 - **Assess turbulent leeside heating within $\pm 30 \text{ W/cm}^2$**
 - **Identify windside heating augmentation within $\pm 30 \text{ W/cm}^2$**
- Only the first two are directly measured with instrumentation.
- All others require **analysis** in-the-loop (Hypersonic Computational Fluid Dynamics, and Ablator material modeling)



Aerothermal Reconstruction

Aerothermal reconstruction requires modeling and ground-based testing for three broad categories:



Aerothermal environments:

- Gas-surface interaction
- Turbulent onset and augmentation**
- Trajectory and atmospheric models
- Gas-phase chemistry
- Blowing and roughness

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Material Response

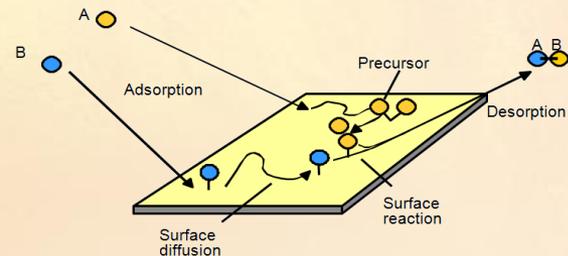
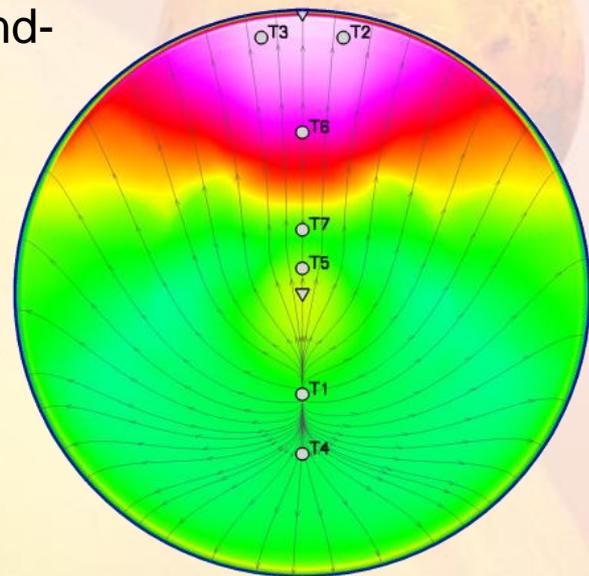
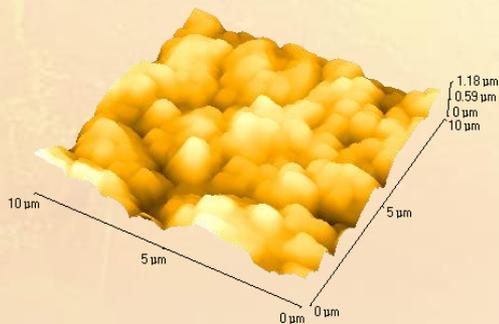
- Virgin properties**
- Char properties**
- Pyrolysis gas chemistry
- Recession uncertainty**

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Sensor Response

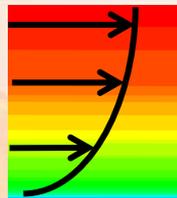
- TC Thermal lag**
- HEAT Calibration
- Noise Filtering
- Response to transient environment

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Aerothermal Analysis

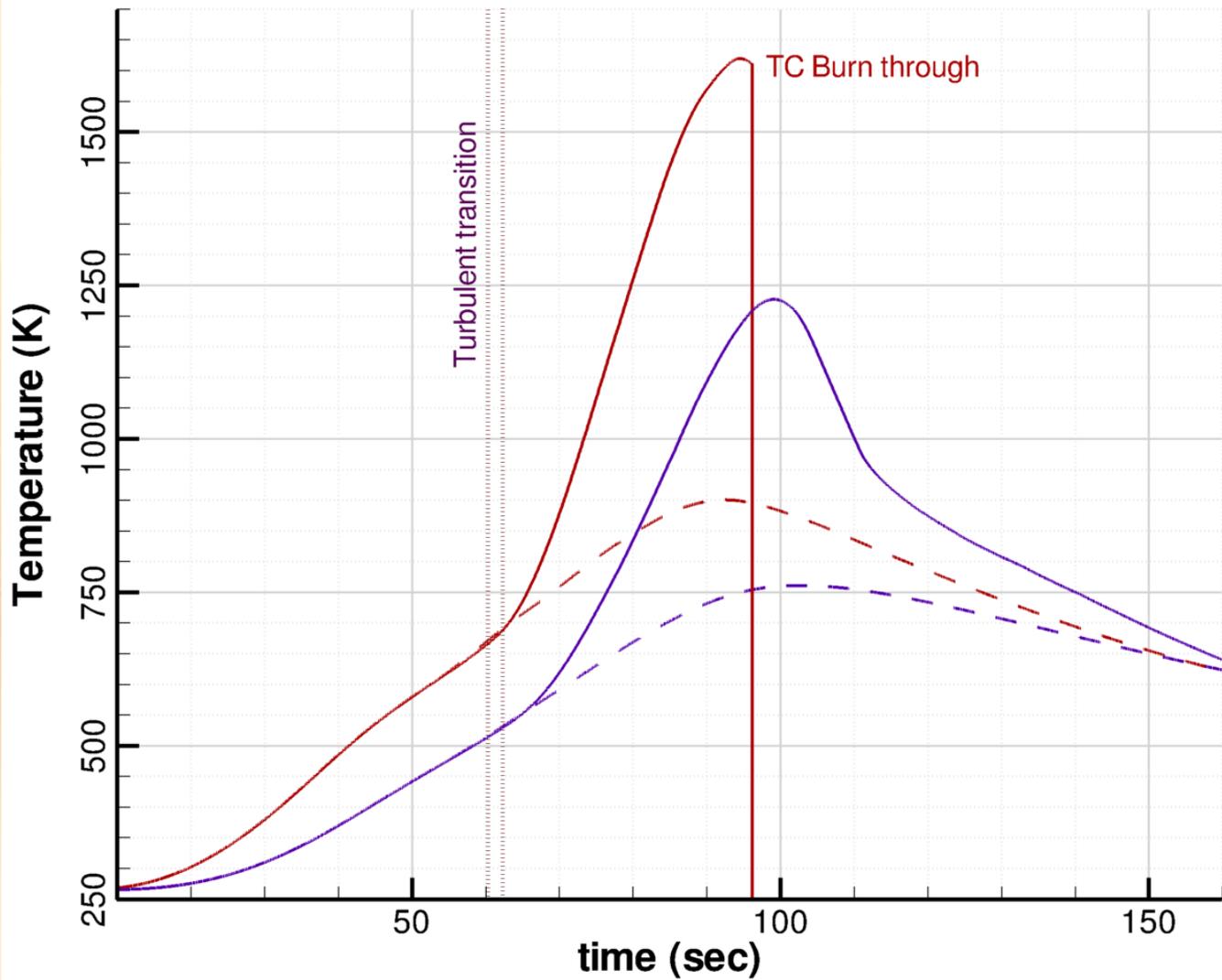


- What is the expected MISP response to turbulent transition and augmentation?
- For a single plug location, the response of top two TCs is shown, for simulated laminar and turbulent environments.
- Turbulent heating leads to a noticeable slope change in TCs particularly close to surface.

MISP2 Simulated Response (DPLR+FIAT)

Comparison between laminar and turbulent environments

— TC at 0.1"
— TC at 0.2"

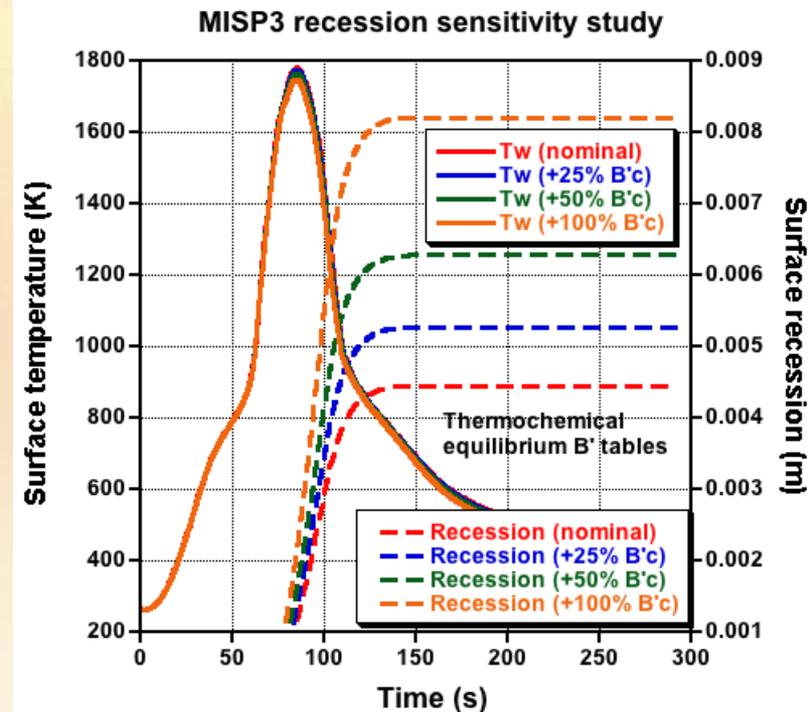
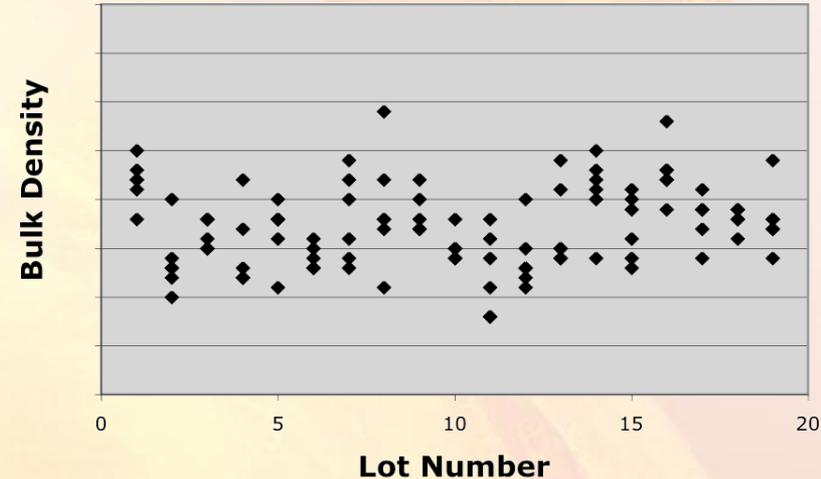




Ablator Modeling and Material properties testing



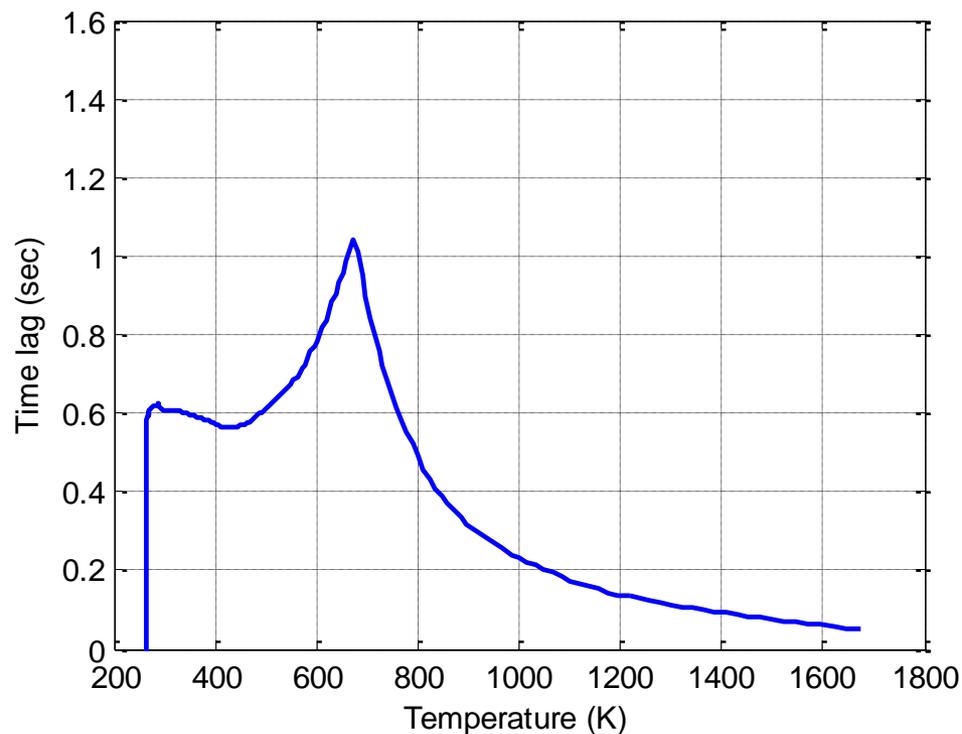
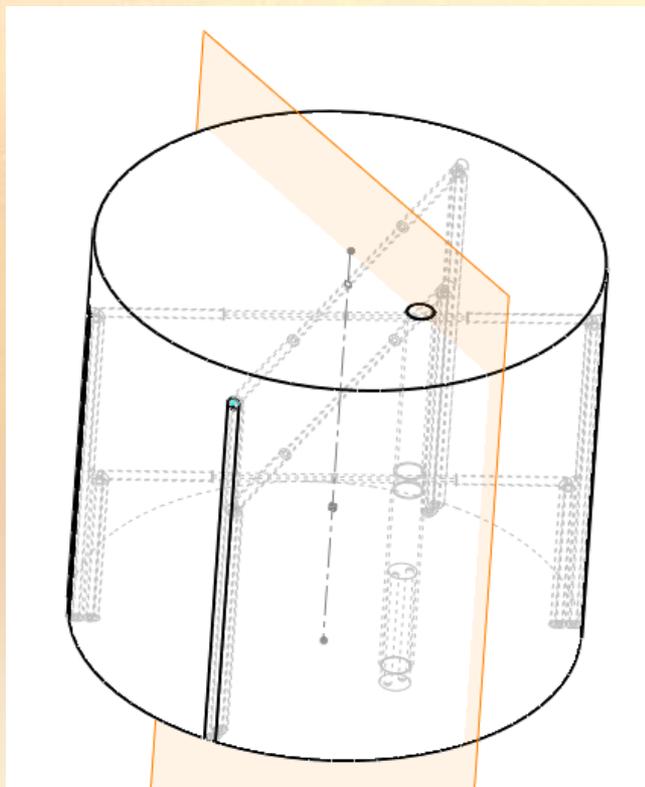
- Existing material models for PICA are intended to cover variability in PICA billets, and in arc-jet tests.
- We are tailoring the PICA model to the material in the sensor plugs, with an emphasis on parameters relating to thermal conduction model (virgin and char ρ , C_p , and k)
- We also are assessing the impact of material modeling uncertainties within our analysis tools.





MISP Sensor Lag

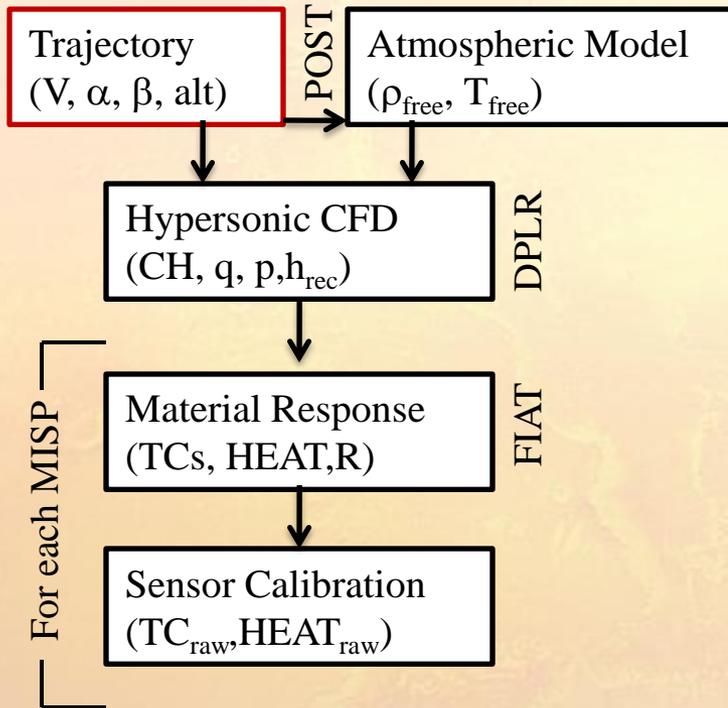
- Thermocouple accuracy is determined from manufacturer's ratings, and current lag has determined from simplified 2D finite element analysis of arc-jet tests.
- Ongoing 3D finite element analysis should provide better understanding of lag, and possible improvements in HEAT calibration.



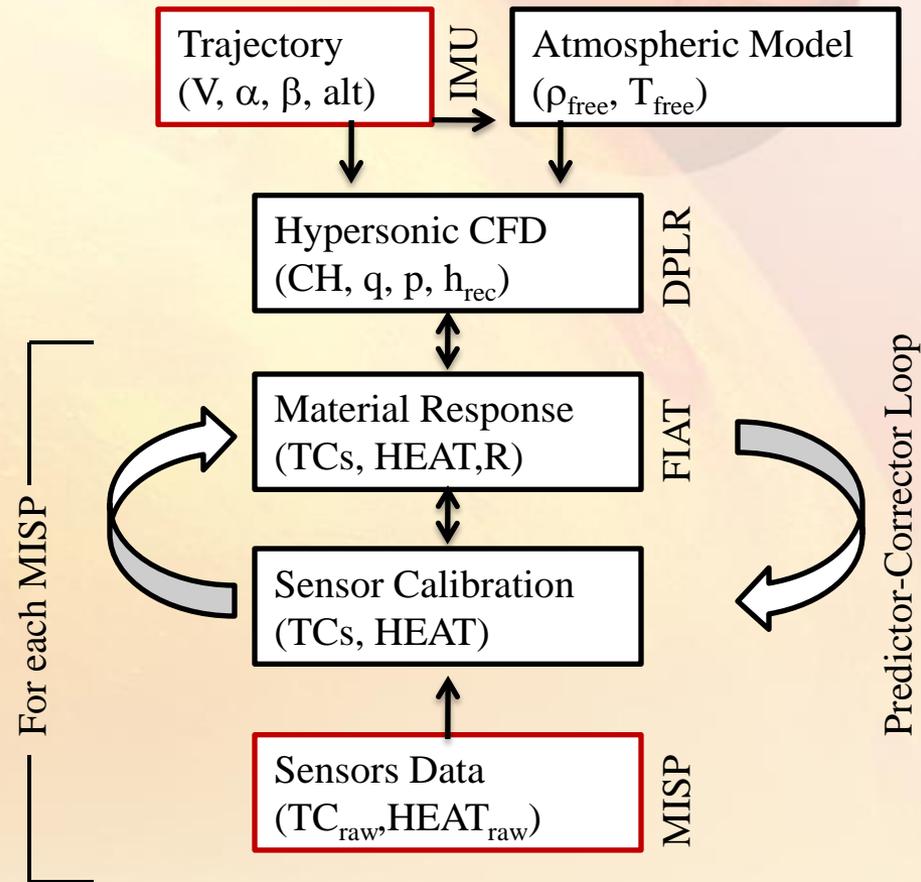


Putting it all together

Direct Process



Process for Flight Data

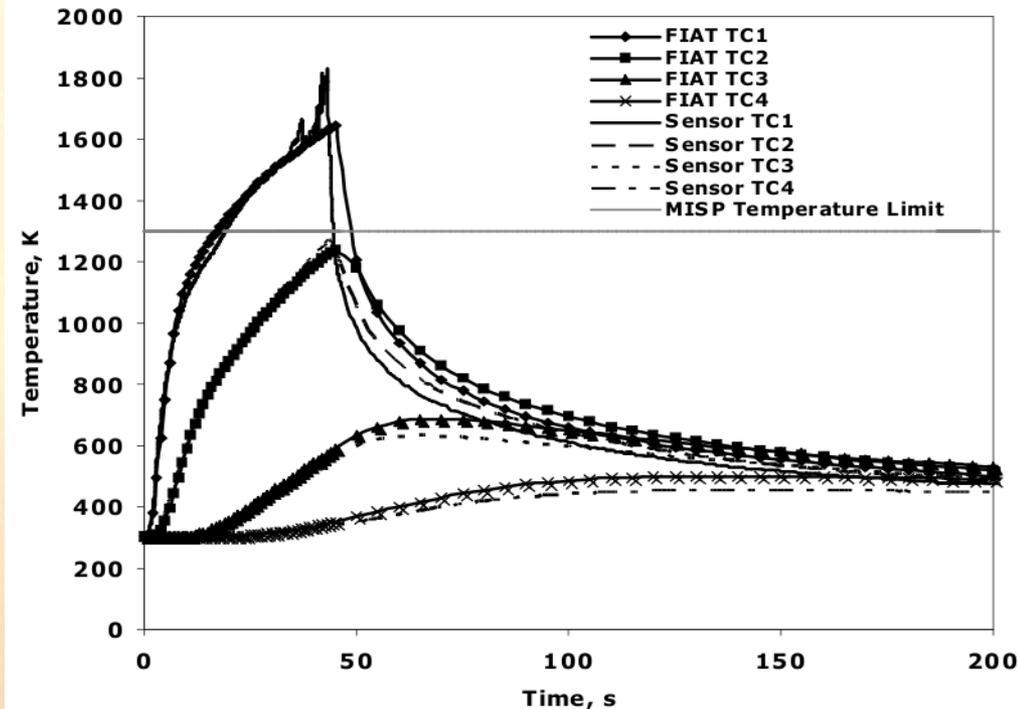


- Direct process akin to vehicle design
- Flight data process needs way to reconcile predicted environments and measured environments
- Analysis step must include model sensitivities.



Predictor-Corrector Development

- Given a **material model**, **four TCs**, and an **isotherm**, how do you recreate in time what happened at the TPS surface (film coefficient, and pressure)?
- Several methods in development:
 - JSC EG3 developing inverse routines for OFT-1 heat shield sensors that searches for CH.
 - Optimization routine wrapped around FIAT (FIAT_Opt), to iterate for CH, and also edge enthalpy, and/or pressure.



- Predictor-Corrector process is limited by:
 - Stability of reverse methodology
 - Quality of input data (susceptible to sensor noise)
 - Applicability of material model



Conclusions & Forward Work

- We need continued aerothermal CFD, material, and sensor analysis, as well as arc-jet and materials properties testing to understand MISP response and MSL environments.
- Imperative to apply analysis tools and methodologies on arc-jet test data.
- Data gathered will be greatly valuable to the aerothermal community, and available for future reconstruction, improvement of tools and methodology.



Acknowledgements

- Thanks to both MEDLI ESMD and MEDLI ARMD projects for their funding of hardware, testing, and reconstruction activities.
- Portions of this work done under contract NNA10DE12C to ERC, Inc and NNA09DB39C to Jacobs Engineering.

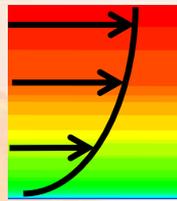


Backup

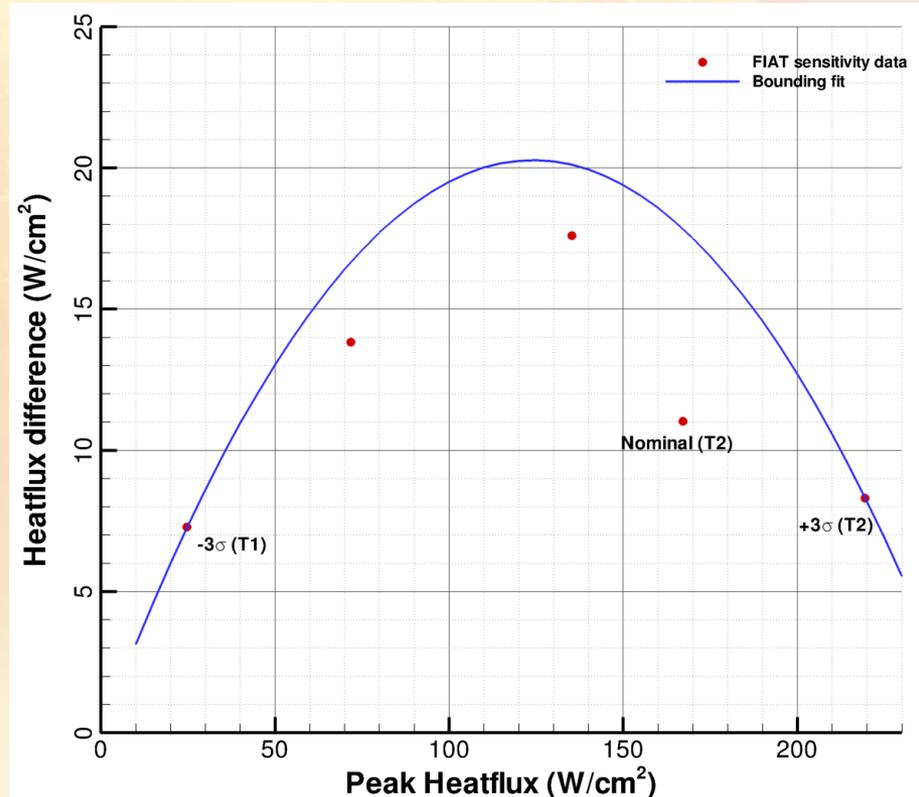
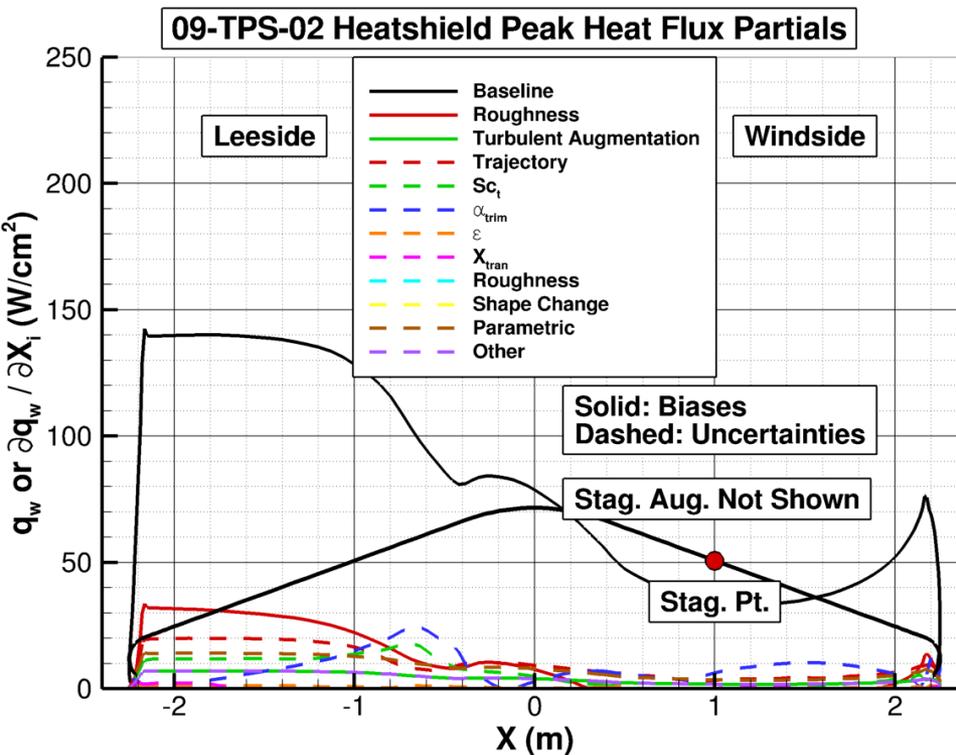




Aerothermal Sensitivities, cont.

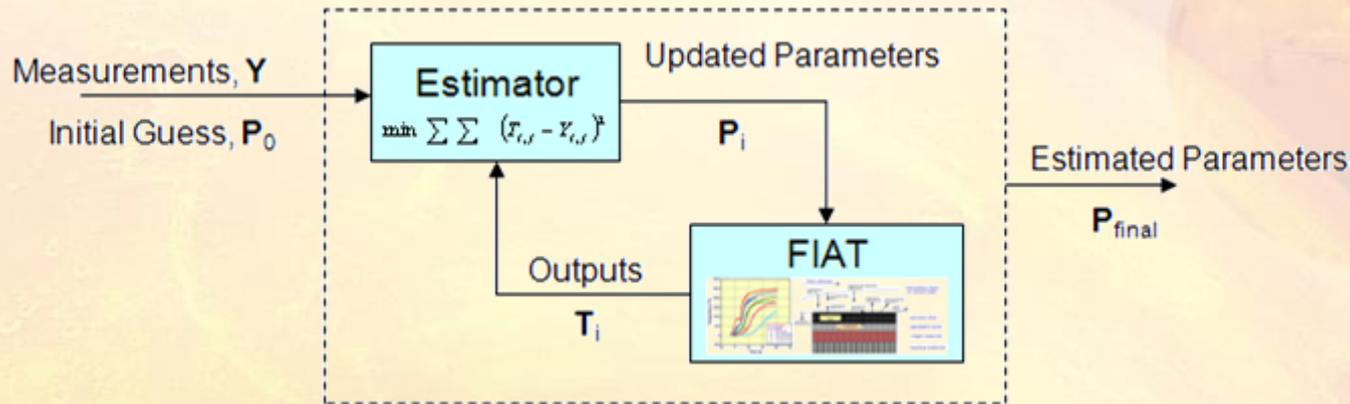


- To assess the overall sensitivity of the sensors to a heating increase, the entire heating pulse is scaled linearly, from -3 sigma to +3 sigma.
- We then extract the minimum change in the peak heatflux that will cause any of the TCs or HEAT to fall outside the known instrument uncertainty .
- This provides a rough sensitivity of the MISP sensors to aerothelmal uncertainties, relative to the peak-heatflux.





Inverse Parameter Estimation approach



Sum of square of errors between measurements and FIAT predictions

- The Inverse Parameter Estimation (IPE) code wraps around FIAT and estimates scaling factors of the input parameters to match measured data via an optimization procedure.
- Code verification
 - Recovers parameters back to the nominal values if starting at a random initial guess
 - Converges to the mathematical minimum of the sum of squares of errors with the experimental data
- Code validation: ArcJet MSL PICA test
- Challenges:
 - Solution existence, uniqueness and process stability
- Minimize errors: ϵ_{model} , ϵ_{random} , ϵ_{bias}

