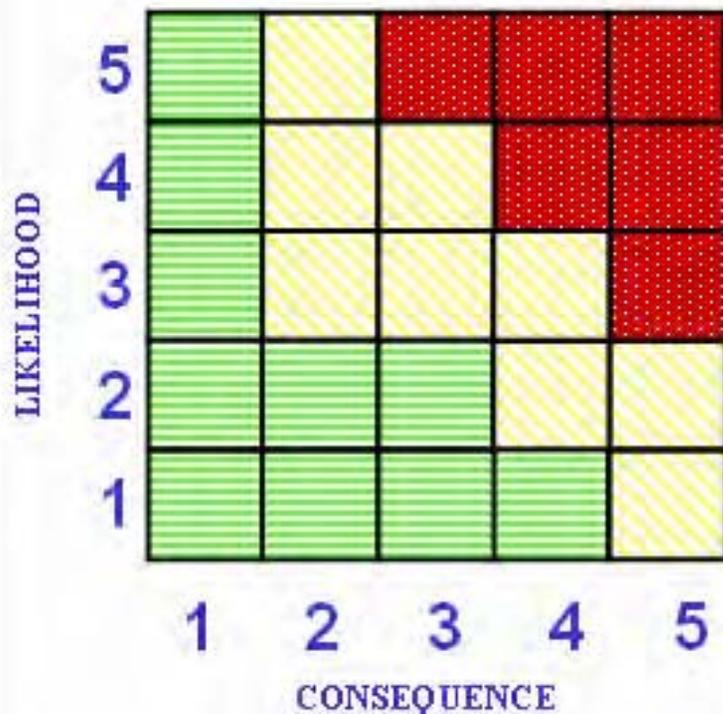


*3rd International
Planetary Probe Workshop
Session 2C*

***HUYGENS
Entry & Descent Analyses
Go-ahead for the Mission***

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ESA-ESTEC, The Netherlands*





Risk Type (either or both may apply to each risk)

Mission Risk Implementation Risk

Consequence of Occurrence

Level Mission Risk Level Definitions

- 5 Complete mission failure
- 4 Partial failure or significant reduction in mission return
- 3 Moderate reduction in mission return
- 2 Small reduction in mission return
- 1 Minimal (or no) impact to mission

Likelihood of Occurrence

Level Likelihood

- 5 Very High
- 4 High
- 3 Moderate
- 2 Low
- 1 Very Low

Aerothermal Analysis Flow



**Aerothermal Analysis Flow
Dominates High Risk Items**

TRAJECTORY &
ATMOSPHERE



THERMAL
ENVIRONMENT
MODELING

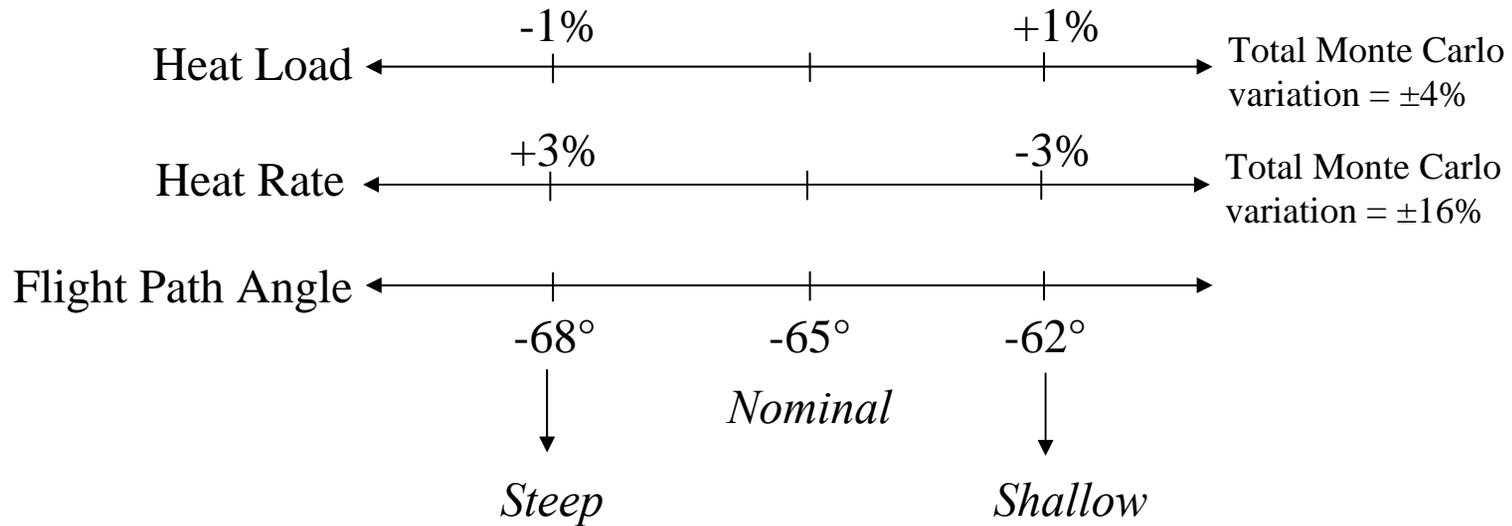


THERMAL
RESPONSE
MODELING



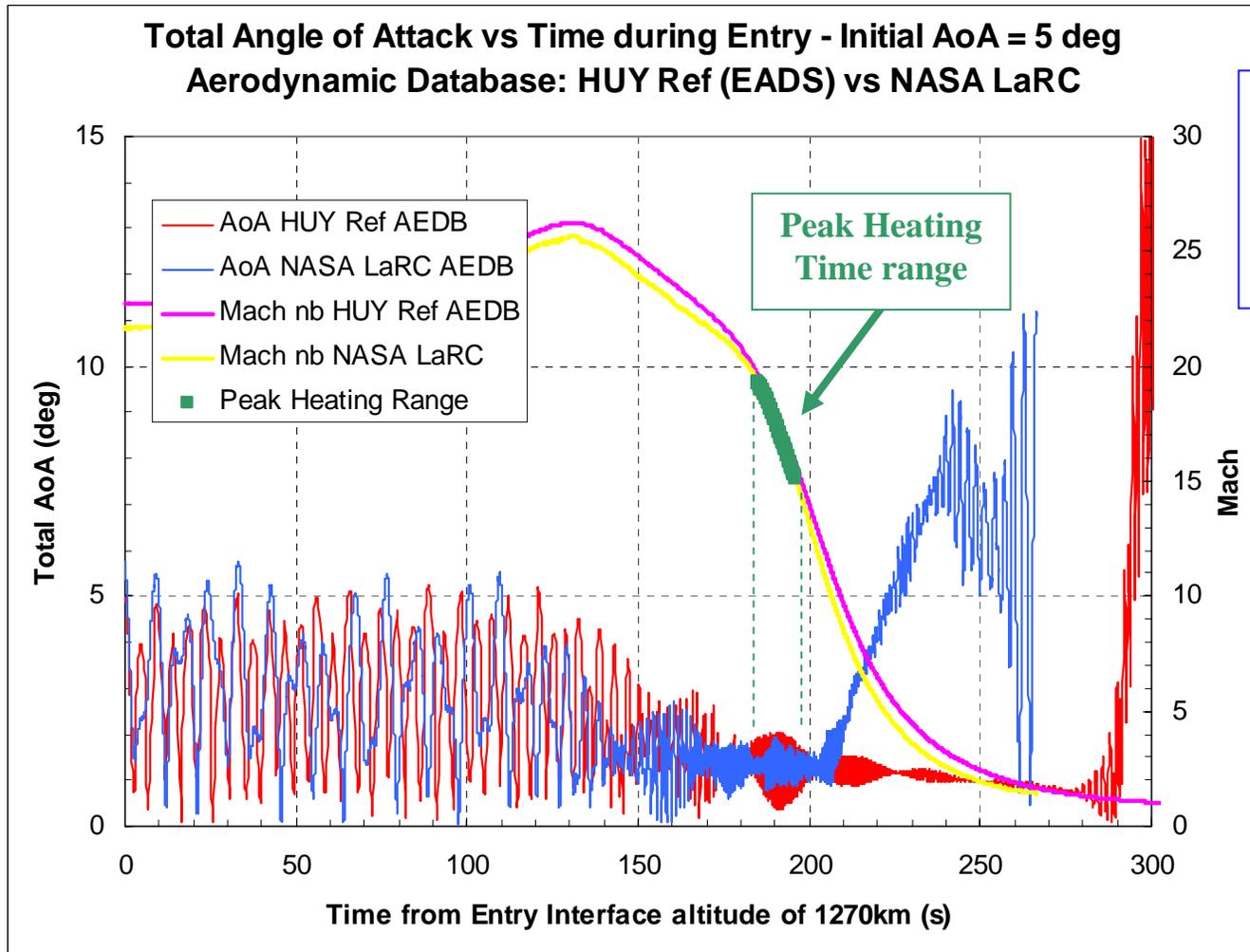
TEMPERATURE
AT CRITICAL
LOCATIONS

Flight Path Angle Effects



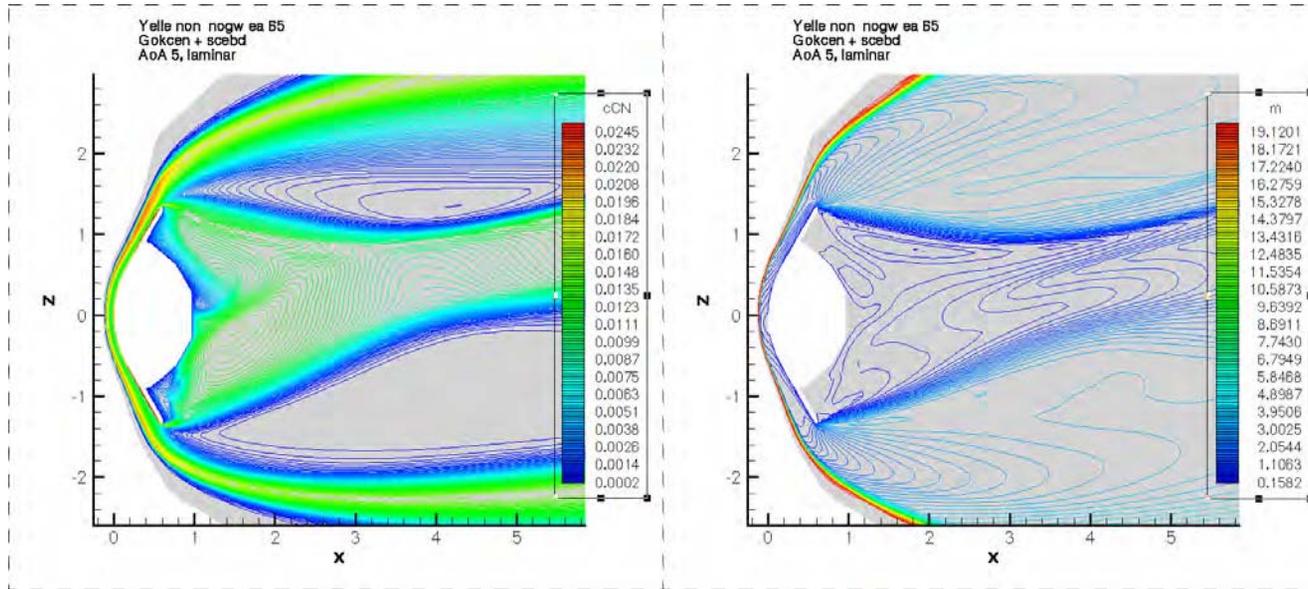
- *High heat rates can lead to material integrity issues such as TPS melting*
- *High heat loads can lead to structural temperatures higher than specification*
- *Most of the variation in performance is caused by the atmosphere*
- *Ability to mitigate heat rate or load concerns by varying flight path angle is extremely limited due to Titan's large atmospheric scale height*

Entry Stability & Angle of Attack Independent Aerodynamic Databases

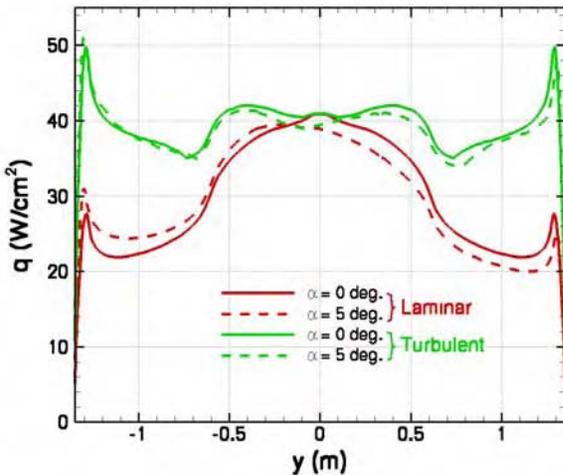


LaRC AEDB
derived from
Genesis

Worst case Angle of Attack (5deg) Impact on Aeroheating



Rnom_NoGW_Ea65, t=187 s

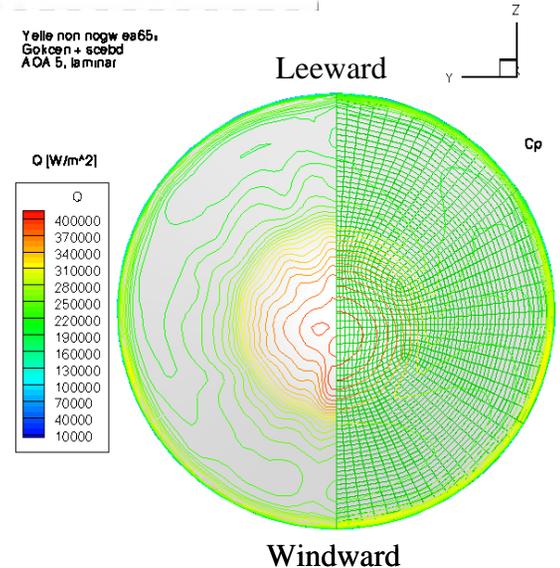


- Laminar heating rate shows expected (small) bias toward windward side
- Minimal impact on turbulent heating rate



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Yelle non noqw ea65, Gokcen + scebd AOA 5, laminar



Uncertainty Factors applied to Boltzmann Heat Flux predictions

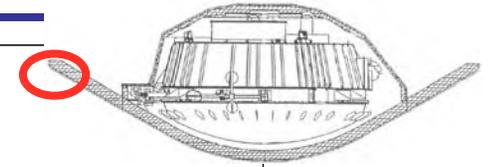


- Full uncertainty factors:
 - Laminar Convective Flux: 15%
 - Turbulent Convective Flux: 40%
 - Radiative Flux: 60%
- Thermal model: 0%, 10%, 20%

Such uncertainties were considered commensurate with understanding of the models and conservatism already applied...

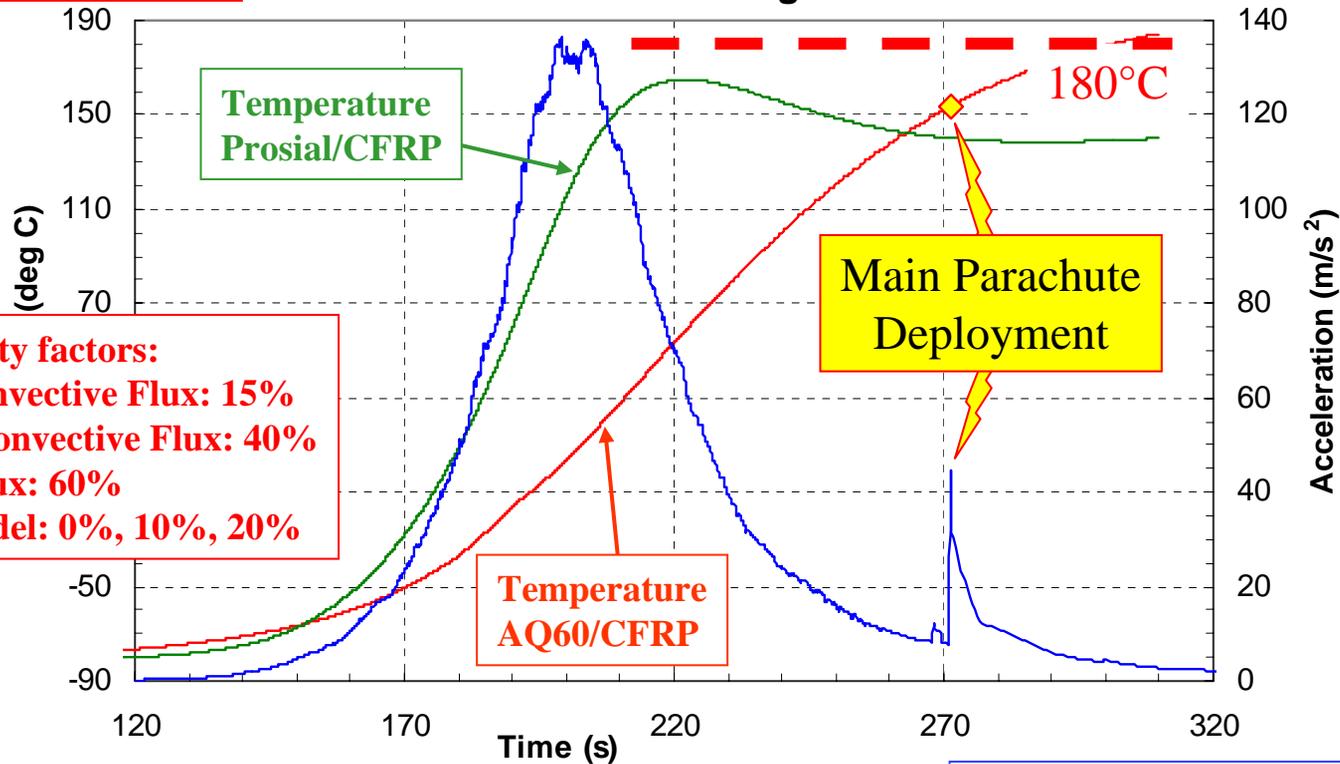
Last Significant mechanical Load on Front Shield

Trajectory LaRC max Heat Load + 1/2 Uncertainty



Decelerator part of Front Shield (Shoulder) is heated on the Front Side and on the Back side...
→ Most critical for TPS thermal Response.

Case B - LaRC Load + 1/2 uncertainty
Development phase Thermal model + 10%
Shoulder Heating



Full uncertainty factors:
 - Laminar Convective Flux: 15%
 - Turbulent Convective Flux: 40%
 - Radiative Flux: 60%
 - Thermal model: 0%, 10%, 20%

Main Parachute Deployment

Monte Carlo 3 σ Trajectory data includes:
 - Titan GRAM Atmosphere Density dispersion
 - Atmosphere Composition with 2.3% CH₄
 - Entry Velocity dispersion Wind included
 - Flight Path Angle dispersion: +/- 3 deg



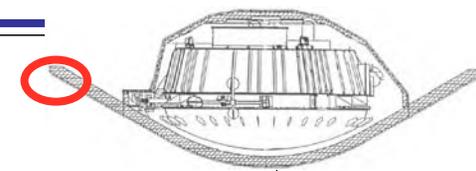
HUYGENS

Case C 10%: LaRC max Heat Load + Full Uncertainty

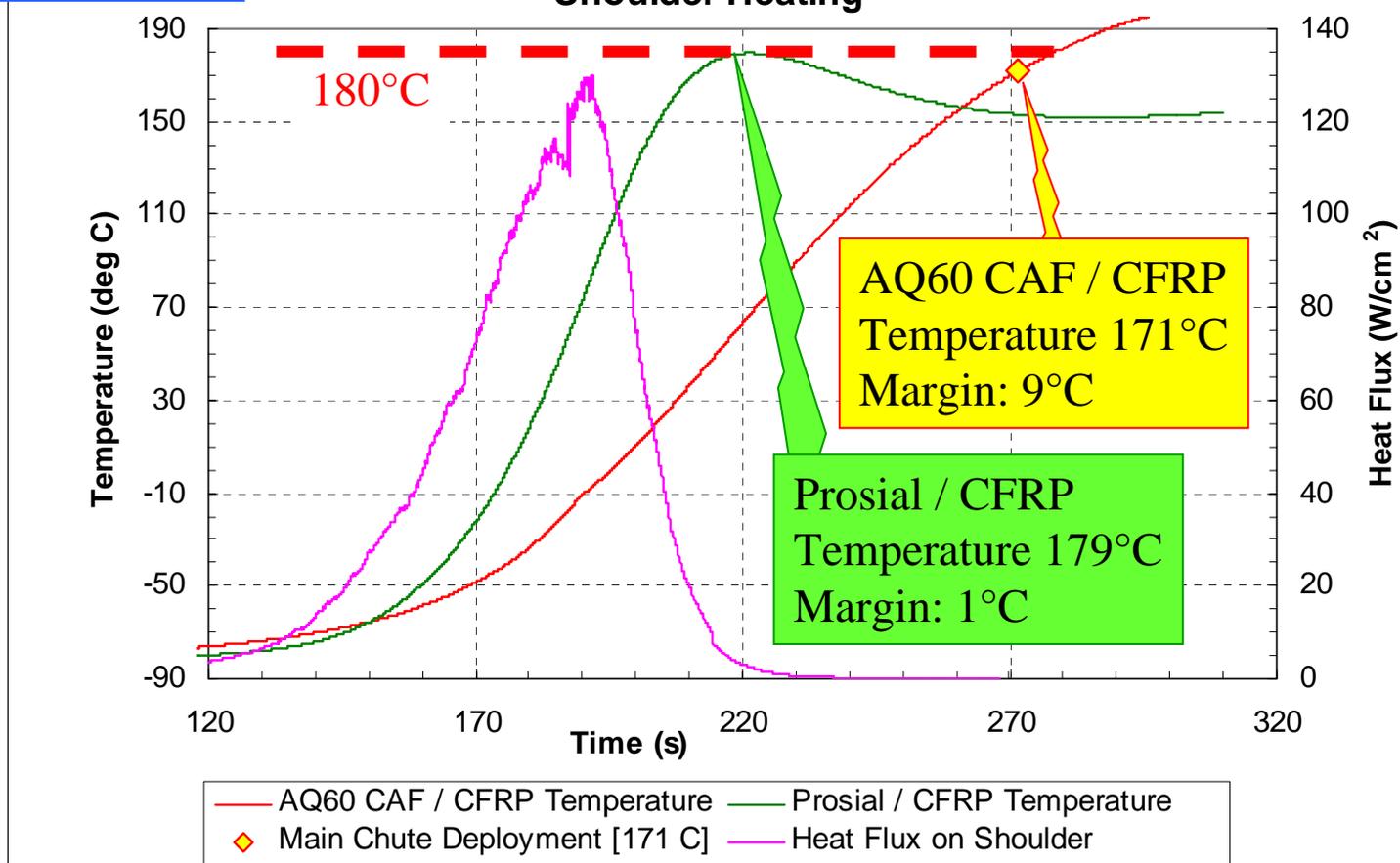
Heat Shield TPS Thermal response to Heat Flux



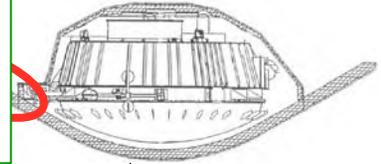
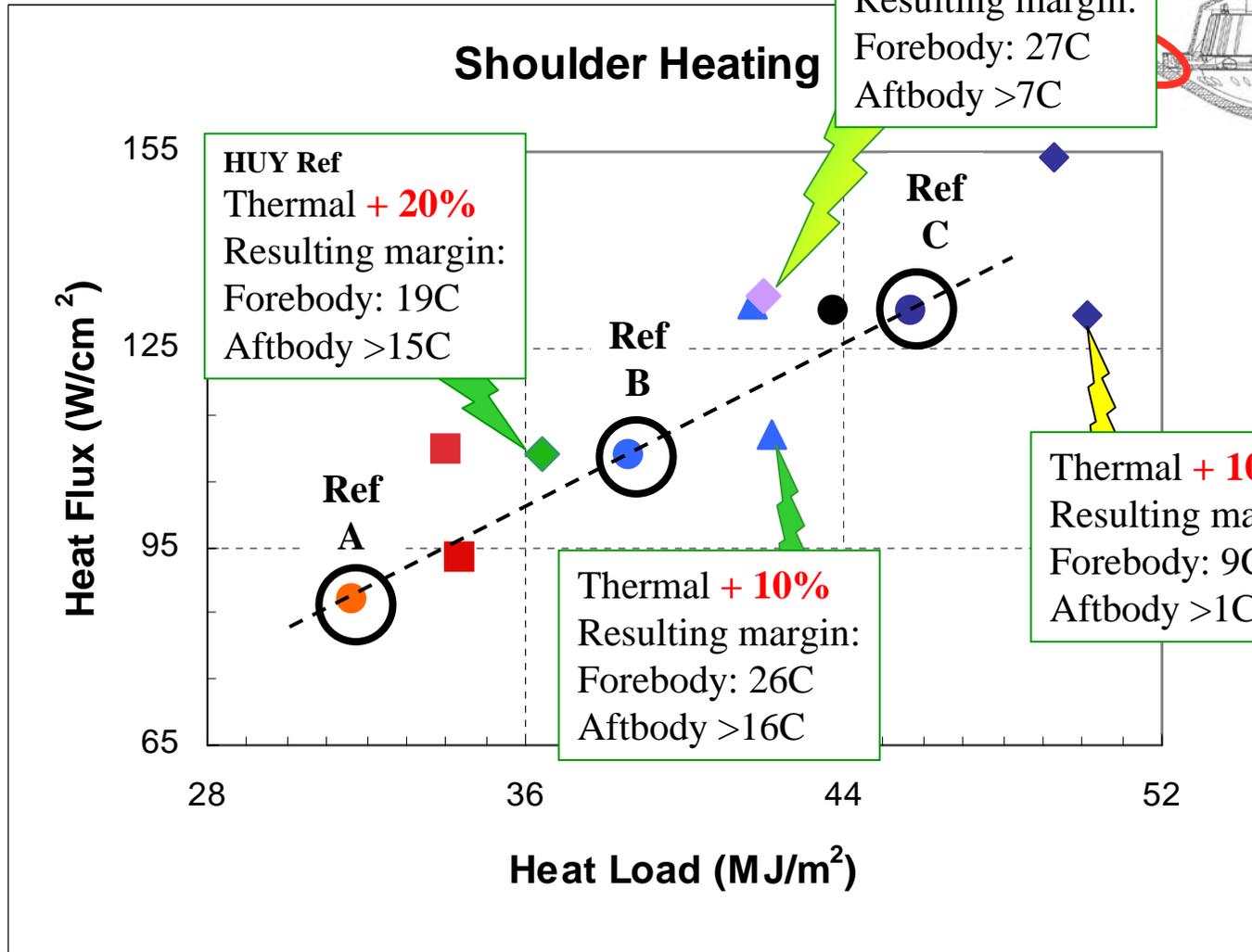
Peak Flux: 130W/cm²
Heat Load: 50.1MJ/m²



Case C - LaRC Load + Full uncertainty
Development phase Thermal model + 10%
Shoulder Heating



Aerothermal TPS Sizing Cases

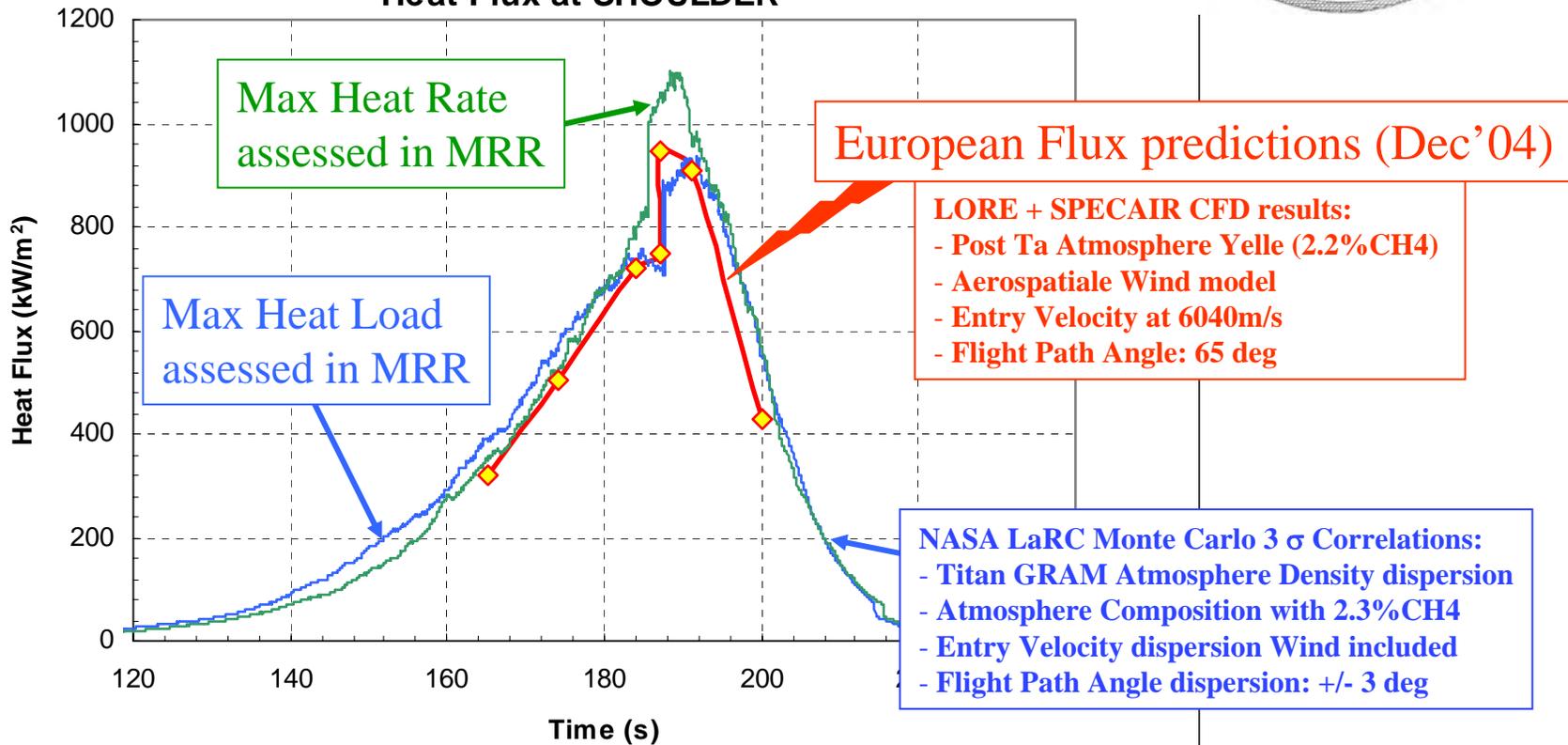
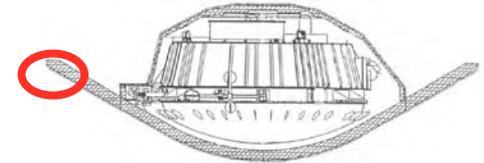


Heat Flux at Shoulder

Most critical element of Front Shield



Post Ta Atmosphere FPA 65 - LORE + SPECAIR
vs Monte Carlo 3 σ - NASA LaRC
Gokcen - Boltzmann 3D - Coupled Tauber
Heat Flux at SHOULDER



Margins Analysis Matrix

Cassini-Huygens MRR – EDL panel Final report



TPS Thermal Response Uncertainty	20%	A20 - Margin* Forebody >19°C Aftbody >15°C	B20 – Margin** Forebody >5°C Aftbody >7°C	C20 – Margin 
	10%	A10 - Margin Comfortable Based on A20	B10 - Margin Forebody: 26°C Aftbody >16°C	C10 - Margin Forebody: 9°C Aftbody >1°C
	0%	A0 - Margin* Forebody >42°C Aftbody >34°C	B0 - Margin Comfortable Based on B10	C0 – Margin*** Forebody >20°C Aftbody >10°C
		None	Half	Full
		<i>Aerothermal Environment Uncertainty</i>		

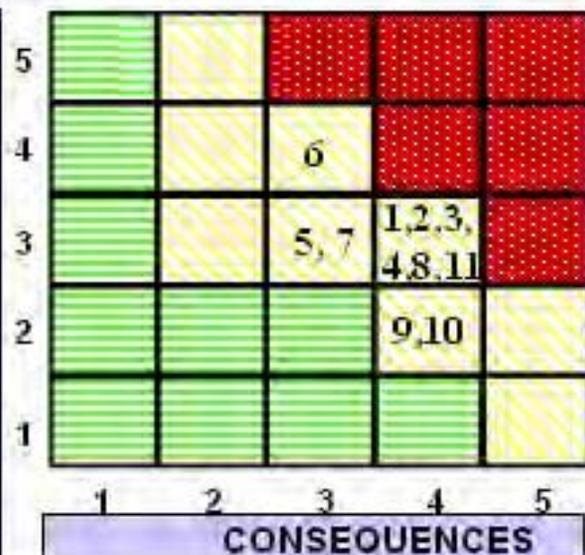
* Case “HUY Ref” + RSS $[(\lambda_1+\lambda_2) \& (\epsilon_1+\epsilon_2)]$

** Derived from B10 results + Thermal model sensitivity

*** Derived from “HUY Ref + ½ uncertainty” + Thermal model sensitivity



LIKELIHOOD



Risk#	ID	Risk	Risk Title
1	T3	High to Mod	Forebody TPS performance not within specification
2	T6	High	Aftbody TPS performance not within specification
4	T5	High	Aftbody TPS thermal response not adequately characterized
3	T2	Med	Forebody TPS thermal response not adequately characterized
5	S3	Med	Unacceptable angle of attack at peak heating increases aerothermal heating effects
6	S10	Med	Probe does not reach ground in specified time and as a result, scientific information may be lost
7	S5	Med	Atmospheric density and composition models and uncertainties do not reflect updated scientific knowledge
8	S6	Med	Wind model and its uncertainty does not reflect updated scientific knowledge
9	A4	Med	Parachute deployment algorithm may malfunction in the presence of atmospheric and/or dynamic transients
10	T1	Med	Forebody thermal environment may not be predicted correctly
11	T4	Med	Aftbody thermal environment may not be predicted correctly

NOTE: EDL panel has been tracking a number of "green" risks, primarily in the avionics, sensors, and algorithms area that were rated green due to high-level evaluation of methodology as opposed to deep penetration. Some of these include things that we are recently sensitive to such as g-switch orientation!

Huygens Atmospheric Entry Validation



Entry validation work covered critical aspects:

- **Probe entry detection mechanism & Parachute deployment**
 - Probe entry acceleration profiles ($80 \text{ m/s}^2 < \text{Peak Acc} < 196 \text{ m/s}^2$)
 - Pyro Arming and Firing ranges ($T_a = 9.48 \text{ m/s}^2$, $T_0 = 10 \text{ m/s}^2 + 6.375 \text{ sec}$)
 - On-board computers Inter-Chain Delay ($< 2 \text{ sec}$ to cover failure modes)
 - Probe stability at parachute deployment ($\text{AoA} < 20 \text{ deg}$ at Pilot firing)
 - Pilot and Main Parachute deployment Loads (Mach & P_{DYN} dependant)
(Pilot $< 2100 \text{ N}$, Main $< 17600 \text{ N}$)
- **Probe entry Aerothermal environment predictions**
 - Peak Heat Flux during entry ($< 1500 \text{ kW/m}^2$)
 - Maximum Heat Load during entry (order of 40 to 45 MJ/m^2)
 - Probe TPS Thermal Response (Front-Shield inner structure $< 180^\circ\text{C}$)



- Despite being scheduled late and concluded less than a month before nominal Cassini/Huygens Separation, the **Mission Risk Review** brought a useful **independent assessment** of EDL predicted performances.
- Amongst other issues, the possibility of a Probe longer descent time was raised...
- Time has been extremely busy in these last months before the mission... and very hot !...
- International cooperation has been most valuable both for ACWG and MRR work...



Final Go-ahead for a 25 December Separation was given on 16 December...!

