

Investigation of a Low Cost Concept for Landing Impact Attenuation

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Roadmap

- Background: Evolution of the ExoMars EDM
- Layout of *Marslander* TDM
- Virtual Test Lab
- Physical Tests
- Conclusions

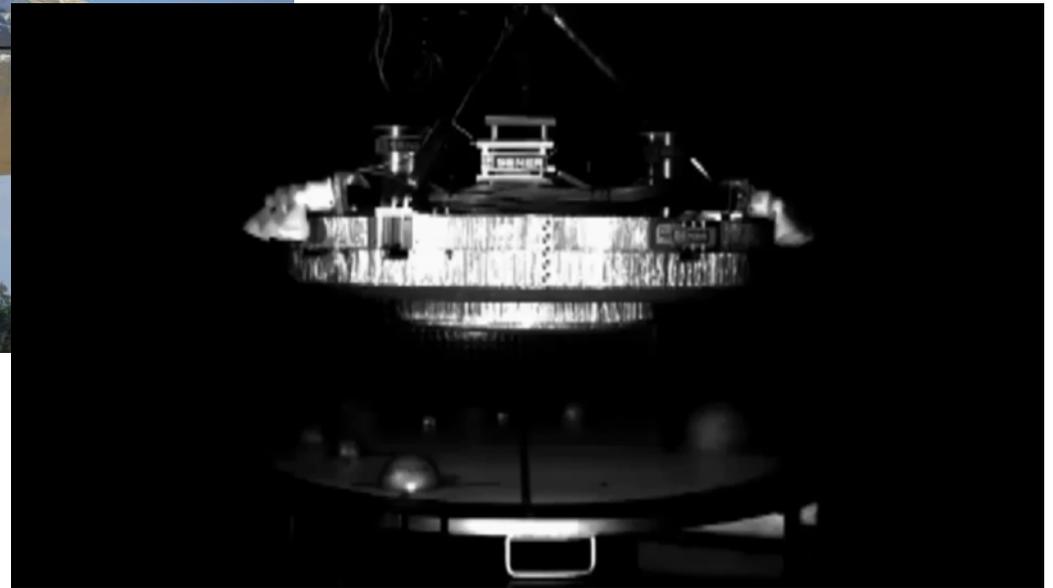
Background ExoMars: Evolution from early Phases to EDM



ExoMars LM in early phases (A... adv. C/D)



Entry, Descent and Landing Demonstrator Module (EDM) of ExoMars Mission 2016

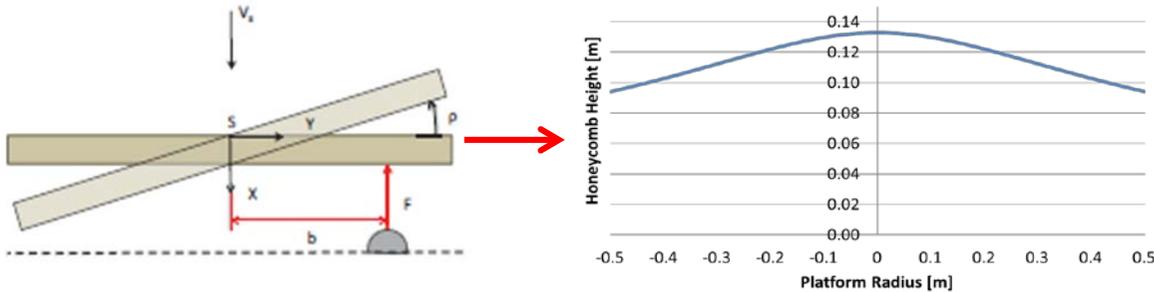


Credits: ESA, TAS-I, Aero Sekur, SENER.... and Airbus DS (former Astrium)

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Guidelines for the *Marslander* TDM - Layout and Physical Tests

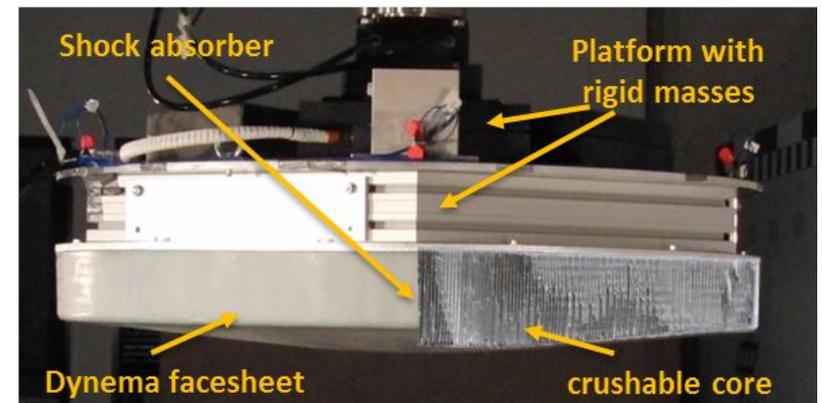
1. Limitation of platform diameter to $<1.25\text{m}$
 - Fits typical automotive crash test barrier size
 - Cheap procurement, already cut into pieces
2. Continuously curved shape based on reduced mass



- Easy to manufacture on a CNC molding cutter
 - Smoothly increasing force instead of plateau
 - Crushable contributes to the spacecraft stiffness
 - Slightly higher layer thickness in the center
3. Rigid test platform with exchangeable crushable
 - No instrumentation on crushable
 - Short changeover times

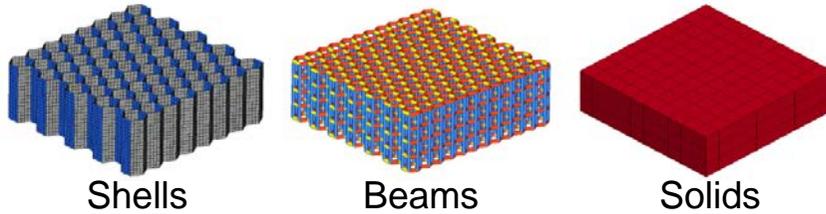
Summary of TDM layout

Mass:	290kg
Moment of Inertia:	$I_1 = 64\text{kgm}^2$ $I_2 = 40\text{kgm}^2$ $I_3 = 40\text{kgm}^2$
Center of Mass:	91mm above crash material
Diameter:	1000 mm
Core Material:	3/16 - 5056 - 0.0007 - 1.0 perforated (Plascore)

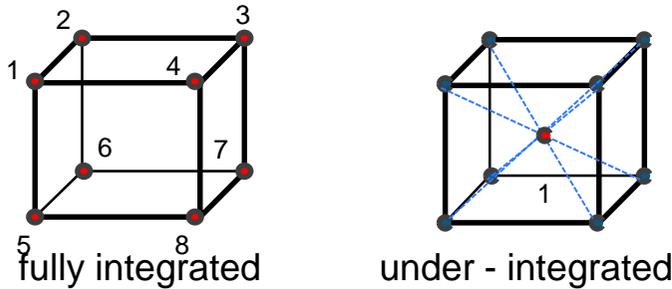


Guidelines for the *Marslander* TDM cont. - Virtual Test Lab

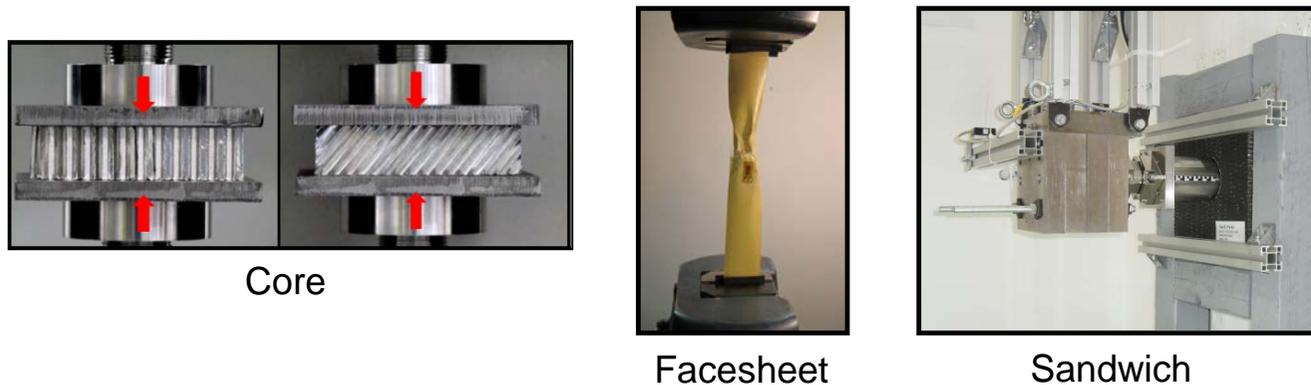
4. Focus on homogenized models (solid elements)



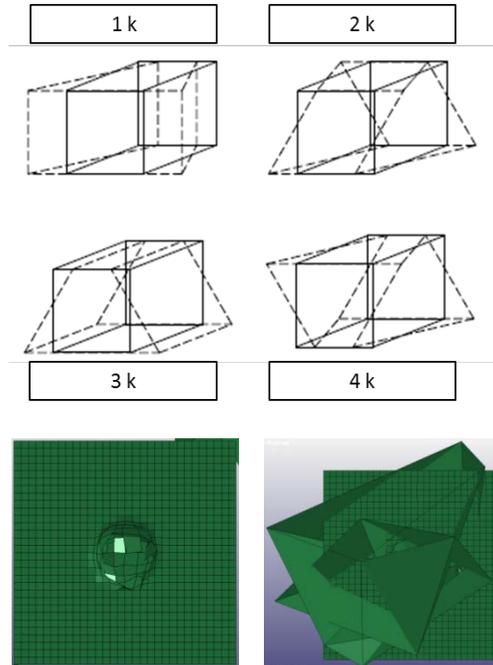
5. Use under-integrated elements (where appropriate)



6. Perform early model correlation tests on low level of integration



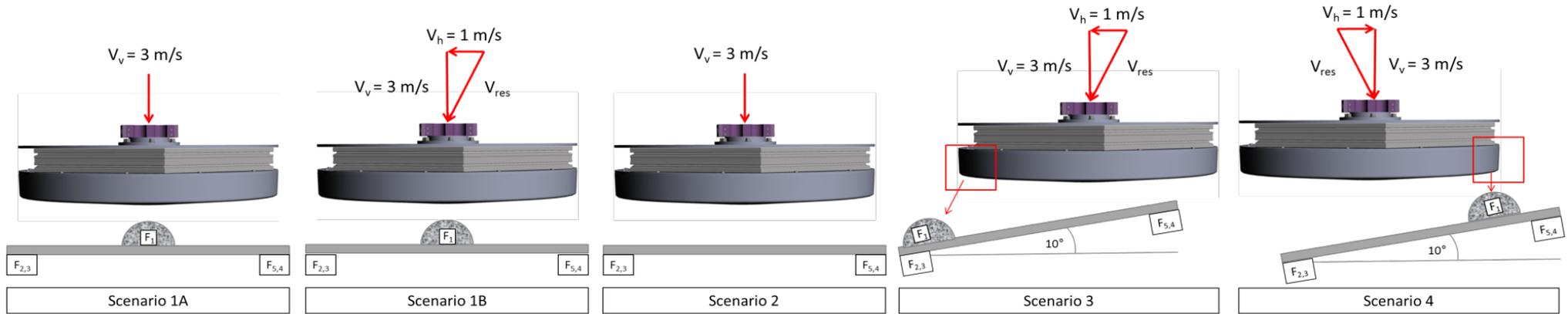
Risk of occurrence of hourglass modes



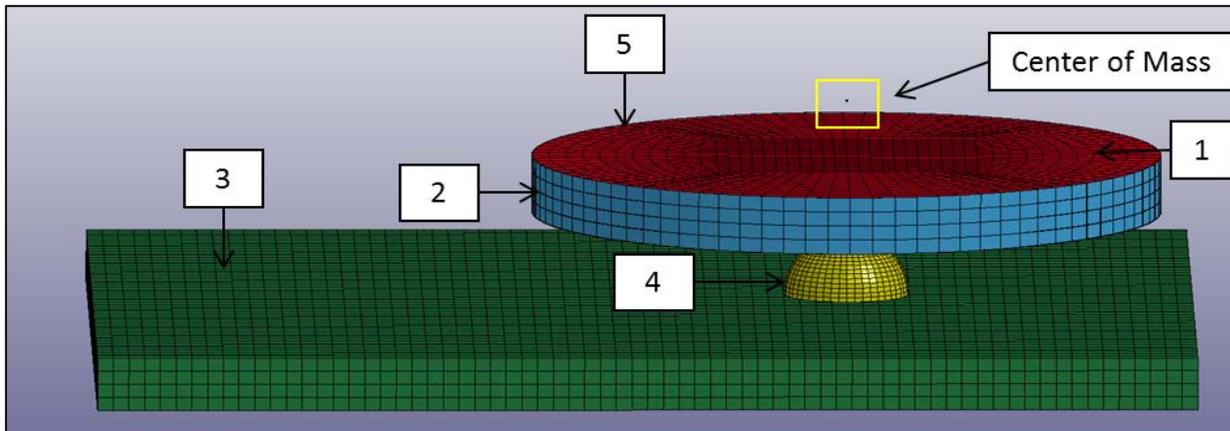
Solution: Introduction of Hourglass control forces
 Target: Hourglass energy <10%

Virtual Test Lab - Test Cases

- Touchdown scenarios:



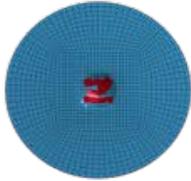
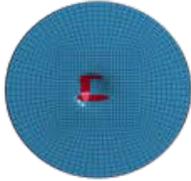
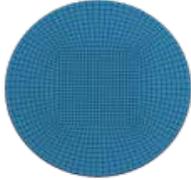
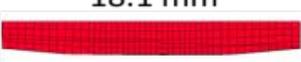
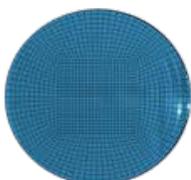
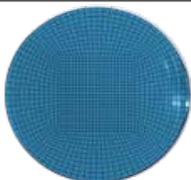
- Numerical Model:



1. Aluminum honeycomb core
2. Dyneema facesheet
3. Rigid ground
4. Rigid stone
5. Rigid plate (virtual)

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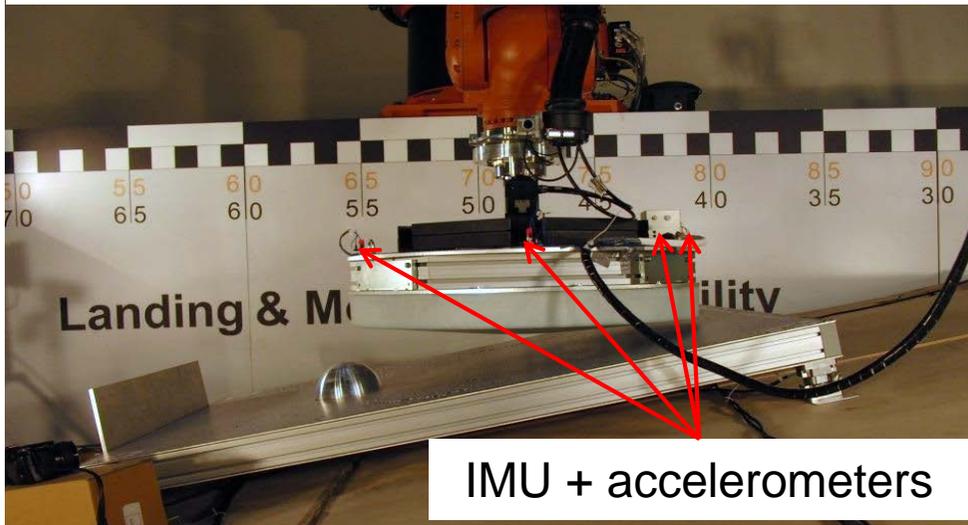
Virtual Test Lab - Summary of Test Predictions

Summary of prediction						
	Deformation	Penetration Depth	Maximal Crash Force	Maximal Acceleration	Hourglass Energy	Total CPU Time
Scenario 1A $v_v = 3\text{m/s}$		74.4mm 	27.8 kN	81.8 m/s ²	4.04 %	6628 s (1h 50min 28s)
Scenario 1B $v_v = 3\text{m/s}$ $v_h = 1\text{m/s}$		68.4 mm 	49.9 kN	151 m/s ²	2.76 %	5865 s (1h 37min 45s)
Scenario 2 $v_v = 3\text{m/s}$		18.1 mm 	166 kN	543 m/s ²	0.18 %	5536 s (1h 32min 16s)
Scenario 3 $v_v = 3\text{m/s}$ $v_h = 1\text{m/s}$			73.7 kN	214 m/s ²	3.75 %	5014 s (1h 23min 34s)
Scenario 4 $v_v = 3\text{m/s}$ $v_h = 1\text{m/s}$			129 kN	415 m/s ²	3.03 %	3794 s (1h 3min 14s)

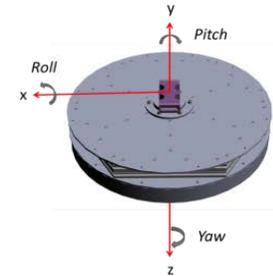
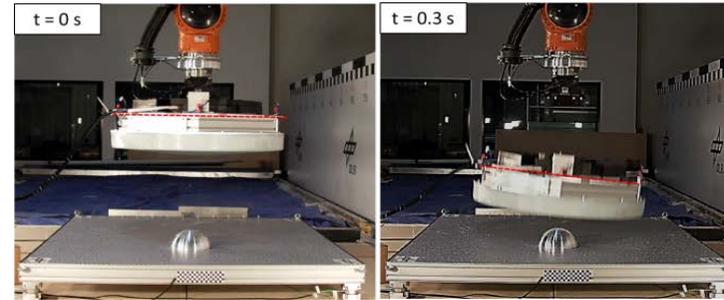
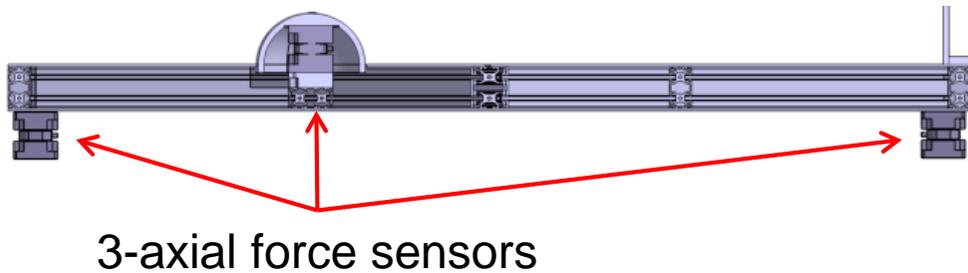
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Physical Test Lab - “the real Test Cases”

Test Set-Up on DLR’s Landing and Mobility Test Facility (LAMA)

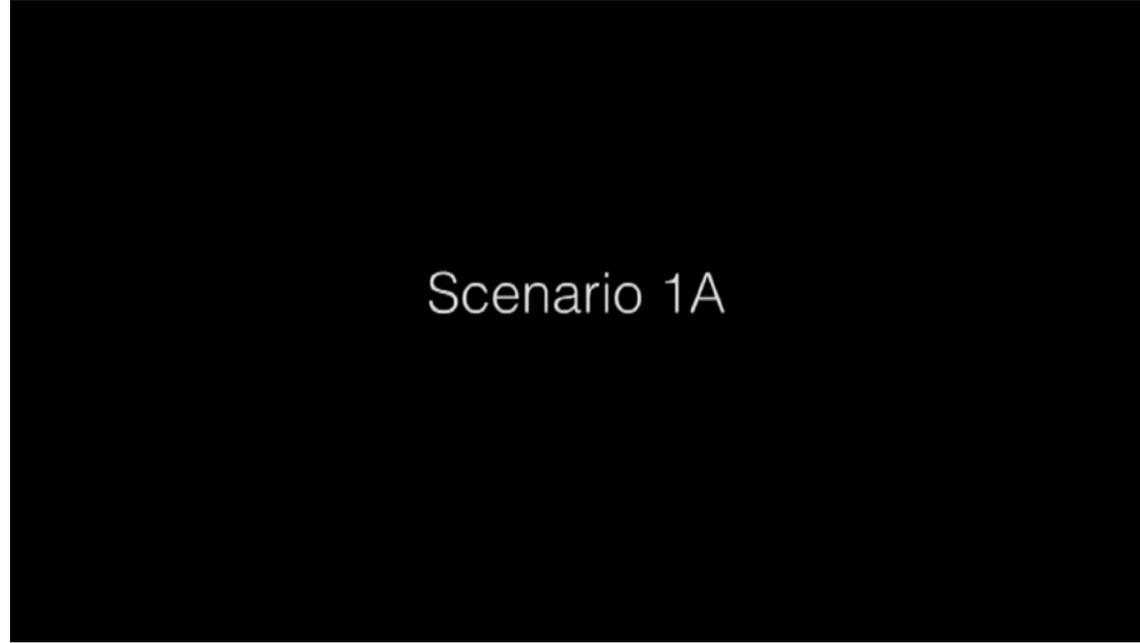
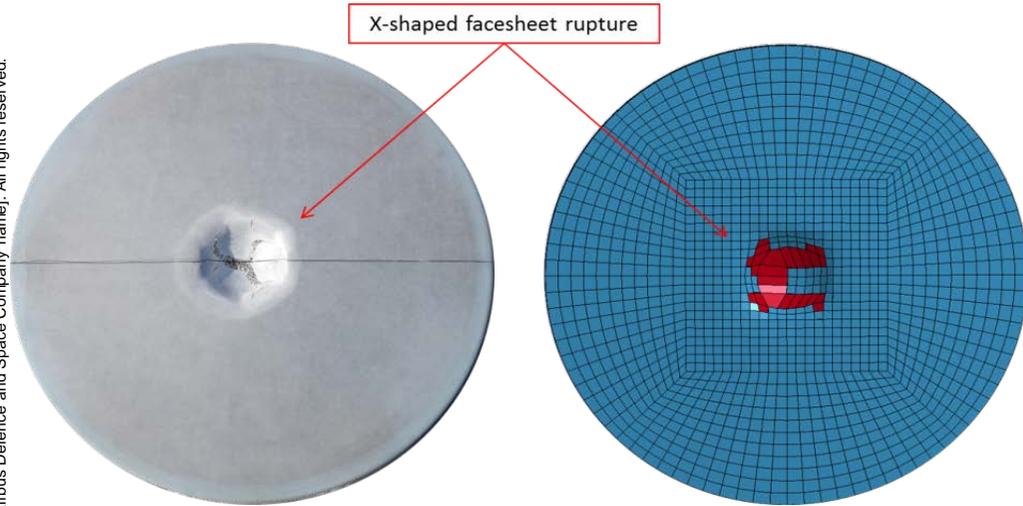


Instrumentation of ground plate

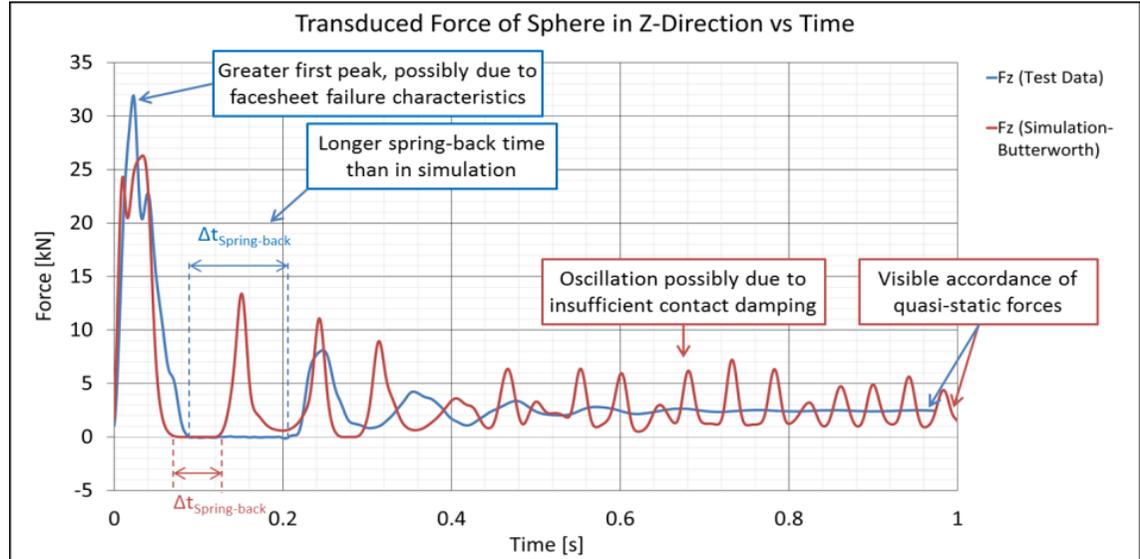
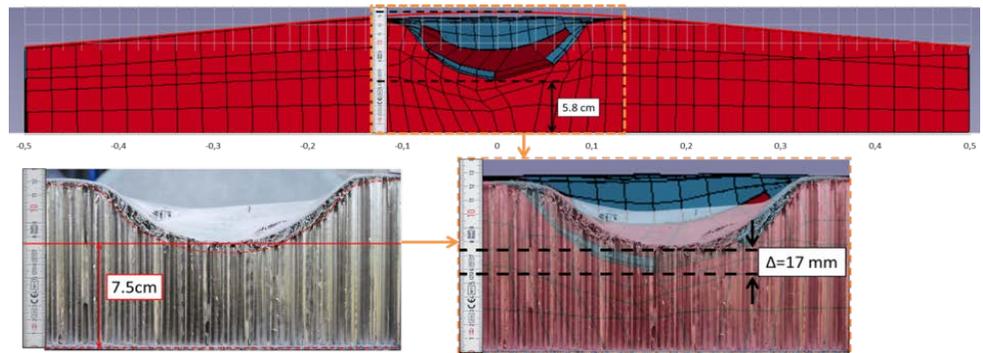


Scenario	Orientation Angle and Angular Velocity at Time of Impact		
1A (Test 2)	Roll: 7.83 deg Pitch: 0.99 deg Yaw: 0.19 deg	$\omega(x) = -0.141$ deg/s $\omega(y) = 19.64$ deg/s $\omega(z) = -1.203$ deg/s	
1B (Test 6)	Roll: 7.34 deg Pitch: 2.36 deg Yaw: 0.12 deg	$\omega(x) = 20.5$ deg/s $\omega(y) = 0.714$ deg/s $\omega(z) = -1.041$ deg/s	
2 (Test 4)	Roll: 6.67 deg Pitch: 1.19 deg Yaw: 0.16 deg	$\omega(x) = 16.32$ deg/s $\omega(y) = -0.225$ deg/s $\omega(z) = -1.14$ deg/s	
3 (Test 7+8)	Test failed due to unhitching of stone		
4 (Test 10)	Roll: 7.22 deg Pitch: 1.7 deg Yaw: -0.55 deg	$\omega(x) = 16.65$ deg/s $\omega(y) = -0.039$ deg/s $\omega(z) = -1.026$ deg/s	

Validation - Scenario 1A

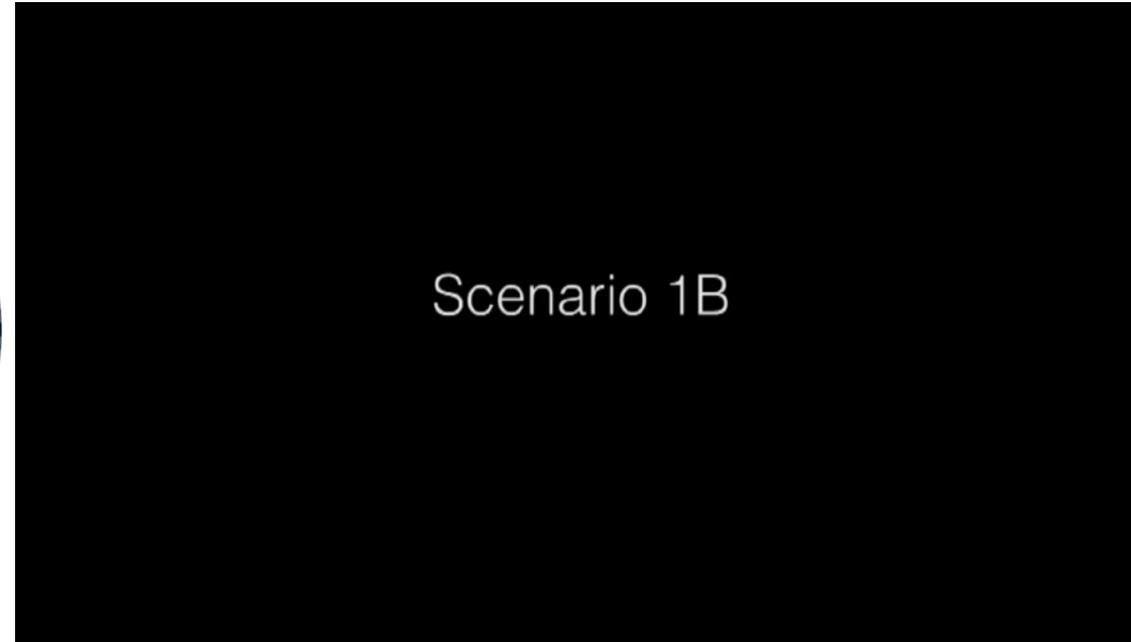
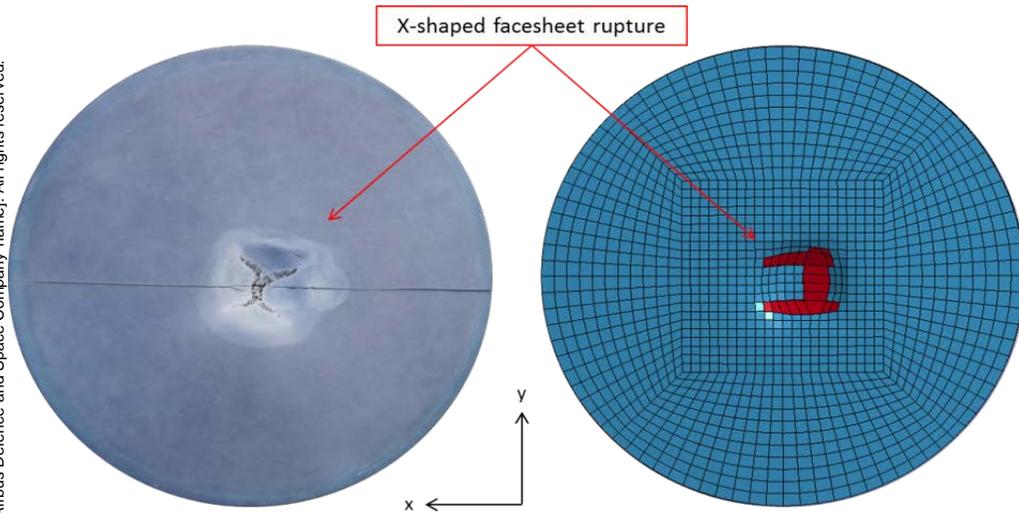


Penetration Depth: $\Delta=17\text{mm}$	
Test: 59.2 mm	Simulation: 76.2 mm

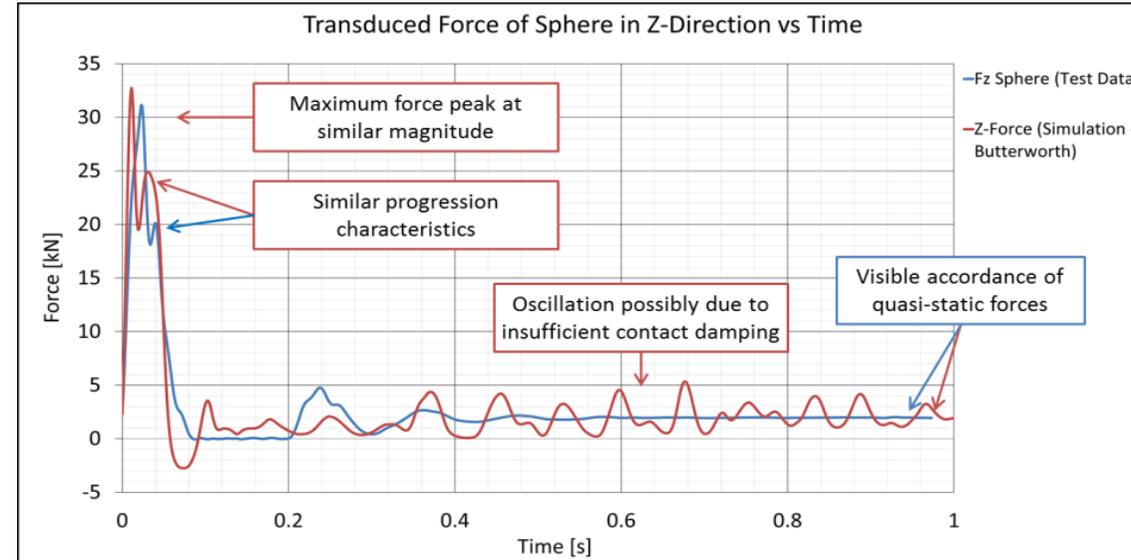
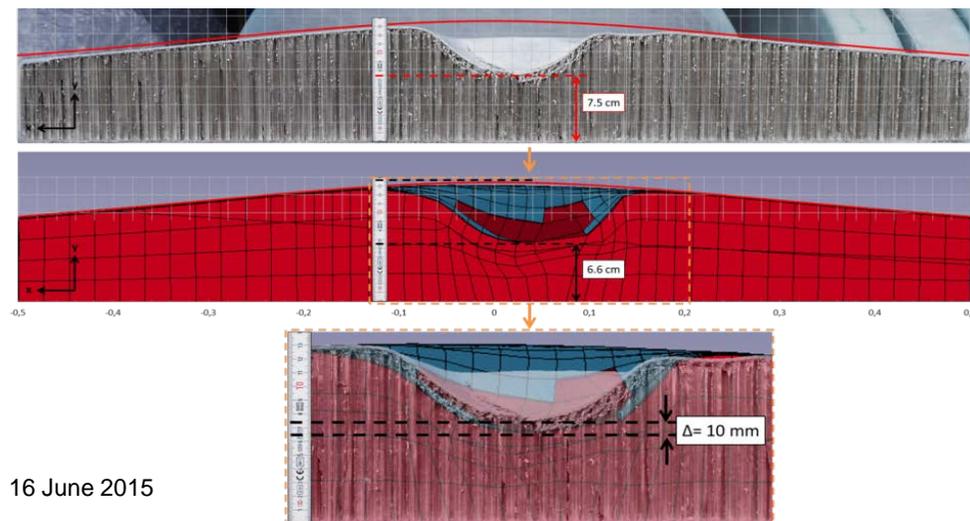


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Validation - Scenario 1B



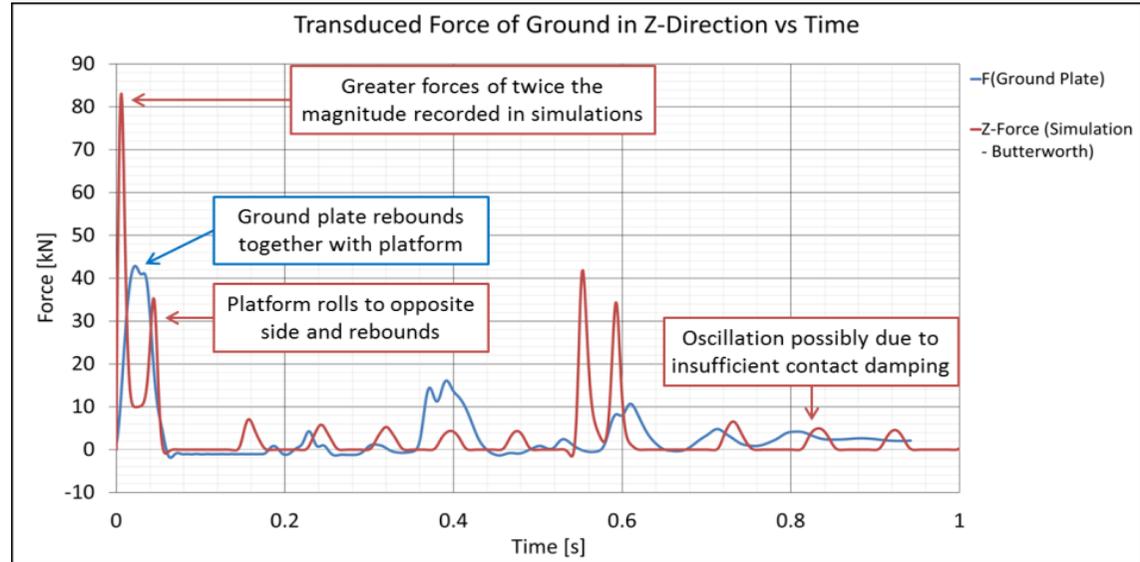
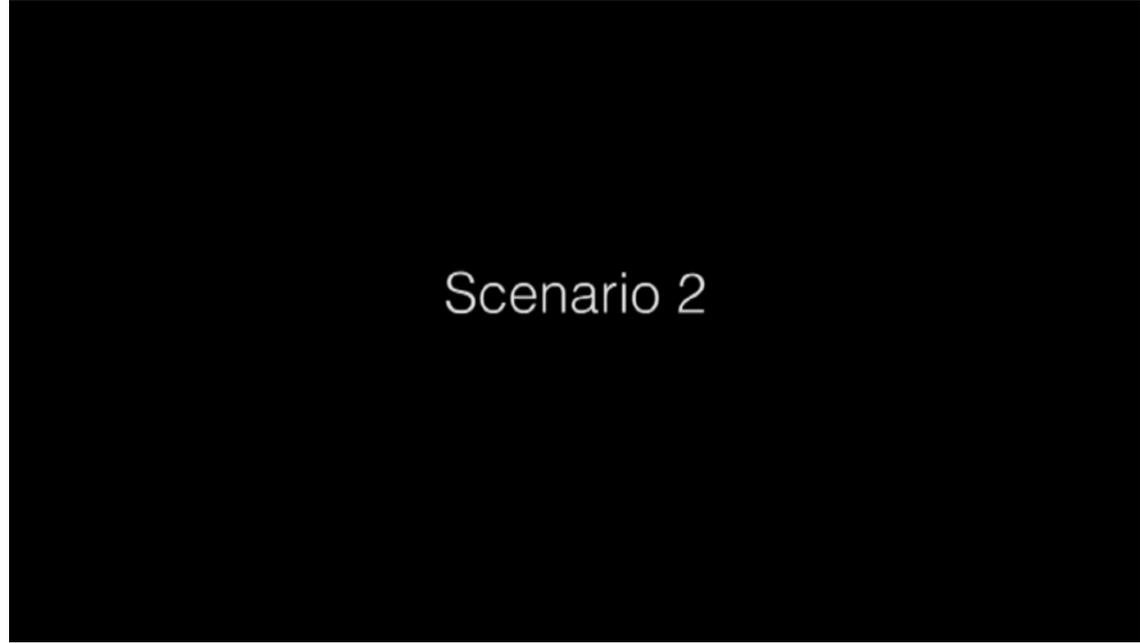
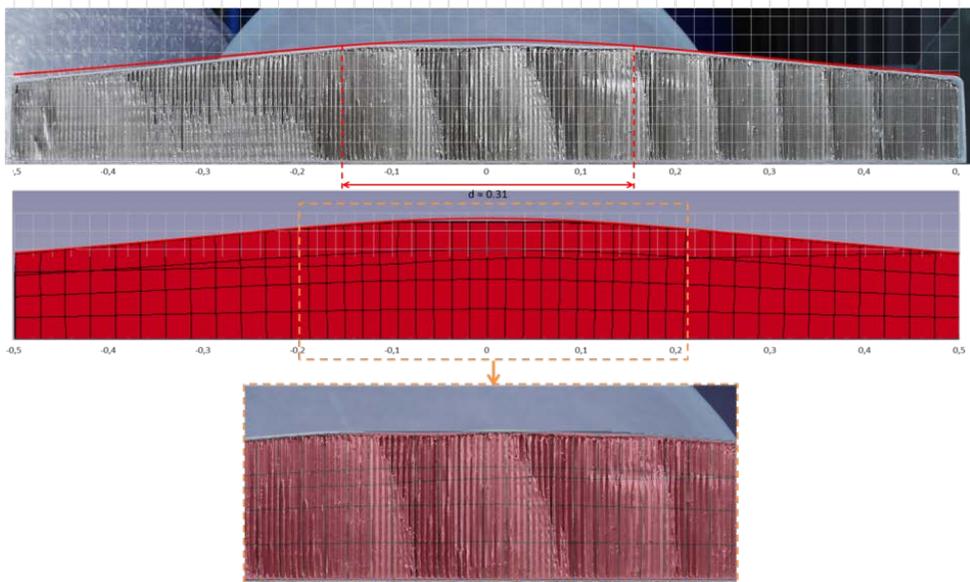
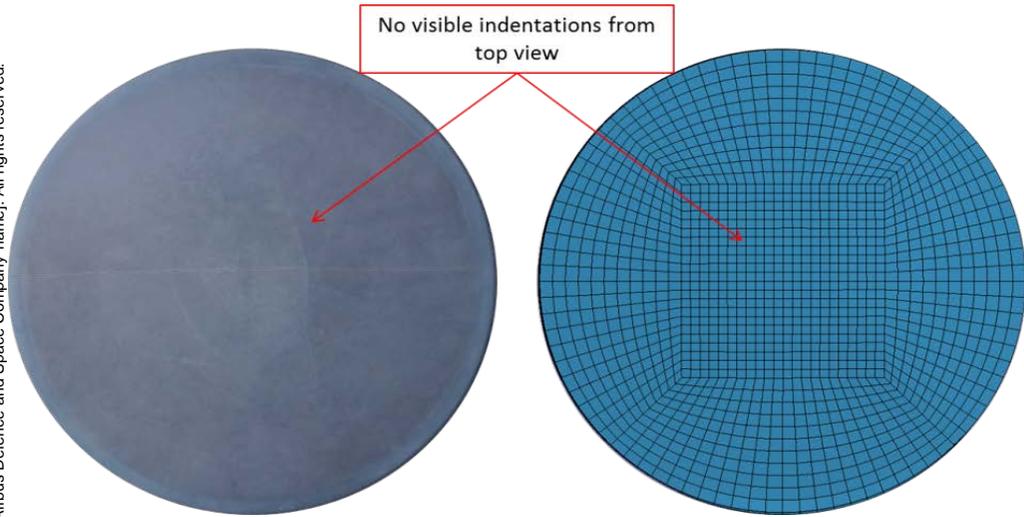
Penetration Depth: $\Delta=10\text{mm}$	
Test: 59.2 mm	Simulation: 68.2 mm



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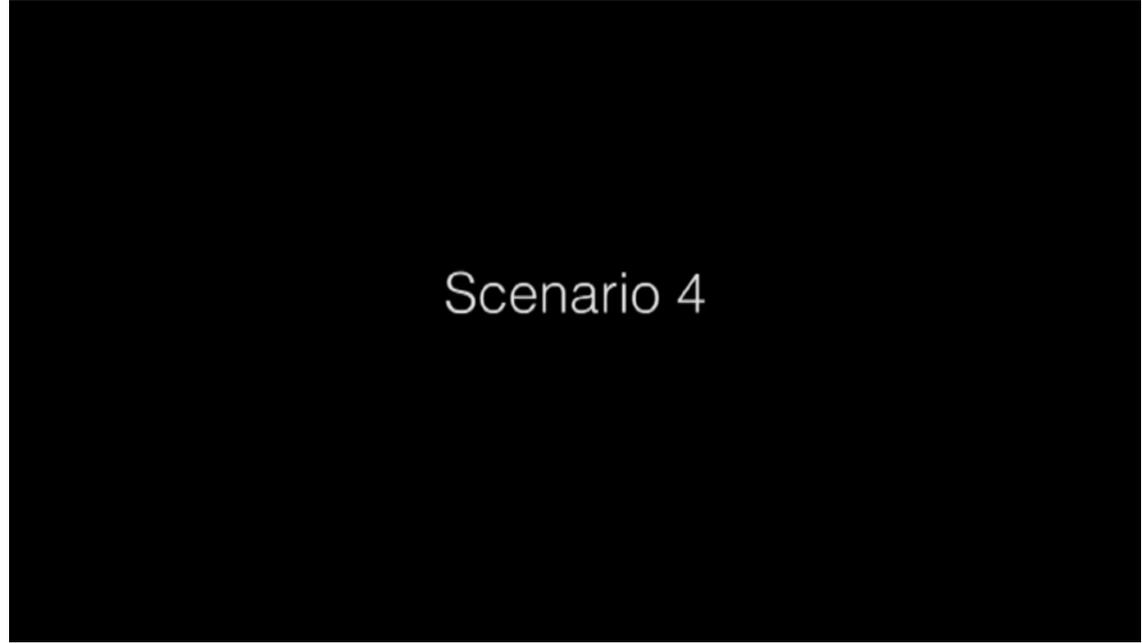
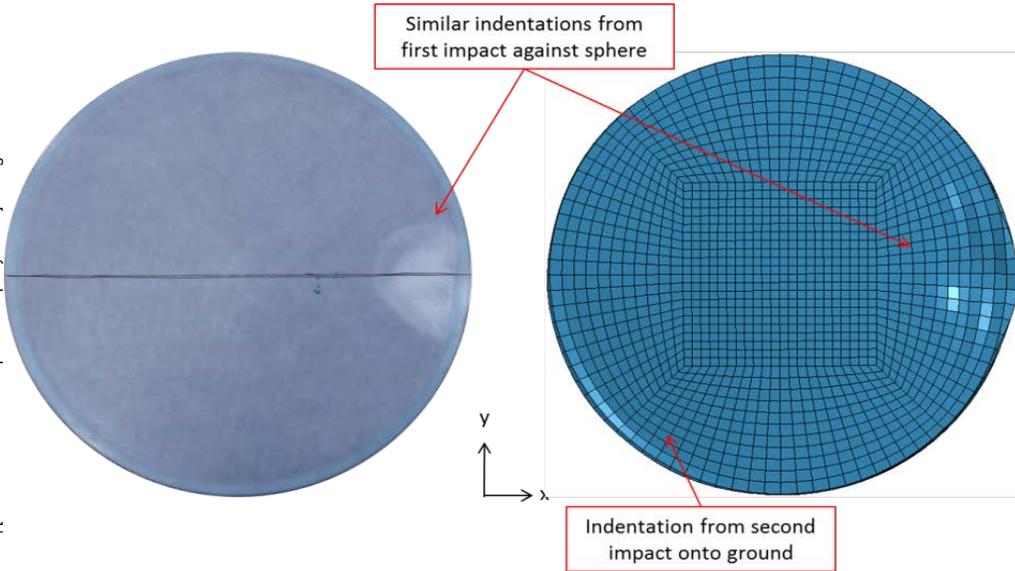
Validation - Scenario 2

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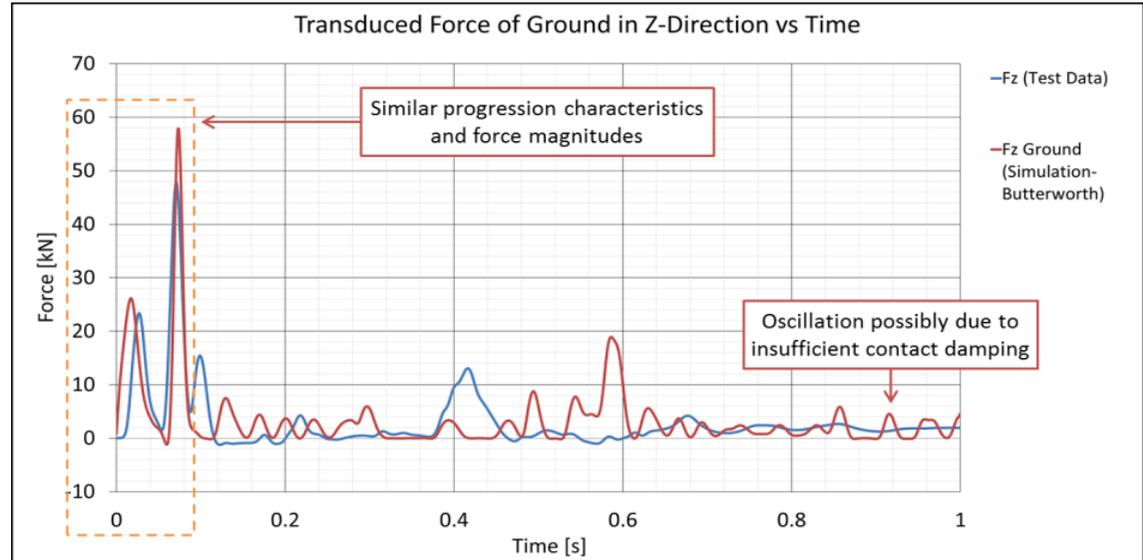
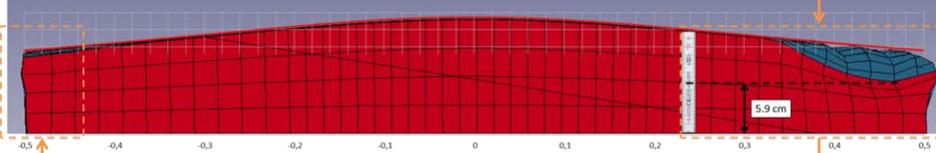
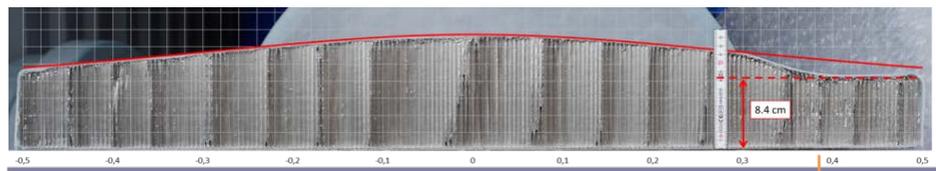


Validation - Scenario 4

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Penetration Depth: $\Delta=25\text{mm}$	
Test: 16 mm	Simulation: 41 mm



Summary and Conclusions

- A cost optimized shock absorber for a landing platform based on a single crushable layer of Aluminum honeycomb has been developed
 - Continuously curved shape
 - Layer thickness based on reduced mass
 - Potentially interesting for missions with several small landers
- 12 specimen have been manufactured and tested under typical touchdown conditions (slopes, rocks, soft soil etc.) at DLR's Landing and Mobility Test Facility (LAMA)
 - Excellent performance under all conditions
- A virtual test lab using homogenized FE models has been established, correlated with material tests (facesheet, core and sandwich) and validated regarding the performed touchdown tests
 - Use of under integrated elements for core material only
 - Simulator over predicts penetration depth and rebound for cases without facesheet failure
 - Correlation based on simple tests led already to surprisingly accurate results at 1.5h CPU time per load case

Acknowledgment

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100% R&D

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