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Future Landing Capabilities of the Mars 2020 Entry, Descent, and Landing System

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Introduction



- 2013 Science Definition Team (SDT) report outlined a mission concept for the Mars 2020 rover, that includes:
 - “...select and store a compelling suite of samples in a returnable cache...”
- Recent studies of approaches to the return of samples from Mars propose a three-mission architecture:
 1. Sample caching rover
 2. **Sample retrieval and launch (SRL) mission**
 3. Sample return orbiter
- Although there are currently no approved plans to return the Mars 2020 sample cache, a future SRL mission would need to access the same landing site as Mars 2020
- Potential challenges:
 - SRL may be heavier than M2020
 - SRL may launch in a poorer opportunity (from an EDL perspective) than M2020
 - SRL may need to be solar powered, due to mass or configuration challenges
- Current desire is for SRL EDL system to be as close as possible to the build-to-print MSL/M2020 EDL system

Study Objectives



1. To understand the impact of a larger landed mass on the heritage MSL/M2020 EDL assumptions and performance
 - Looked at landed masses up to 1200 kg

2. To understand what landing sites can be reached (altitude) by the SRL mission under different arrival seasons and design assumptions
 - Looked at a range of arrival seasons
 - Looked at potential improvements in parachute performance
 - Based on ongoing Low Density Supersonic Decelerator (LDSD) program

Methodology

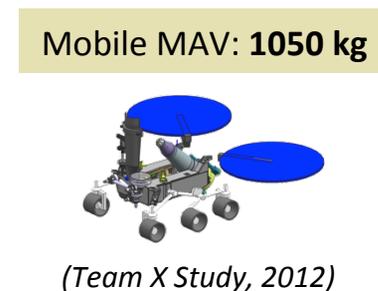
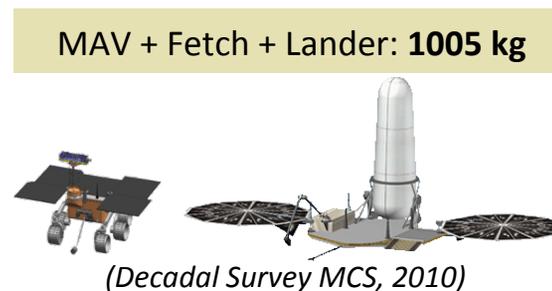
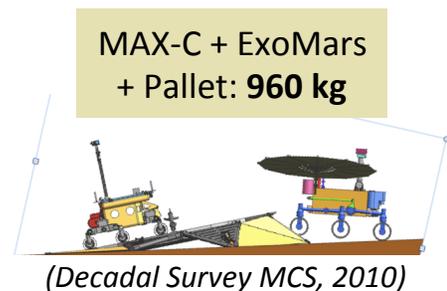


- Simulation approach:
 - Used baseline Mars 2020 assumptions for hardware, software and timeline, vehicle mass properties, and entry interface condition
 - Flew all simulation cases to Gale Crater latitude/longitude and altitude with synthetic terrain
 - Applied seasonal atmosphere assumptions for given Ls
 - Increased landed mass to 1200 kg (no change to non-landed hardware)
 - Evaluated higher Mach parachute deploy (up to Mach 2.4)
- Monte Carlo runs performed for selected arrival dates and parachute deploy Mach numbers
 - Used heritage simulation environment (POST) of the MSL/Mars 2020 EDL team
- Developed partials from the simulation results to extrapolate to other design points
 - Ls sweep: density vs. parachute deploy altitude
 - Mass sweep: ballistic coefficient vs. parachute deploy altitude
 - Terminal velocity: trade timeline margin for landed altitude

Why 1200 kg landed mass?



- Previous EDL studies identified potential fuel margin break point near 1200 kg
 - Current study produced similar results
 - Landing 1200 kg results in ≤ 5 kg of unallocated fuel margin (worst case)
- Preliminary SRL studies suggest 1200 kg is a reasonable upper bound for landed mass



- Additional issues related to landed 1200 kg with current EDL system
 - Available volume and packaging concerns
 - Powered Descent Vehicle (PDV) modes
 - May require redesign of parts of the EDL system (e.g., descent brake portion of BUD)
 - Mobility and touchdown performance capabilities

Drivers on Landed Elevation Capability



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Mars Formulation

1 Landed mass

- ~1 km effect from 900 kg to 1200 kg

2 Arrival season

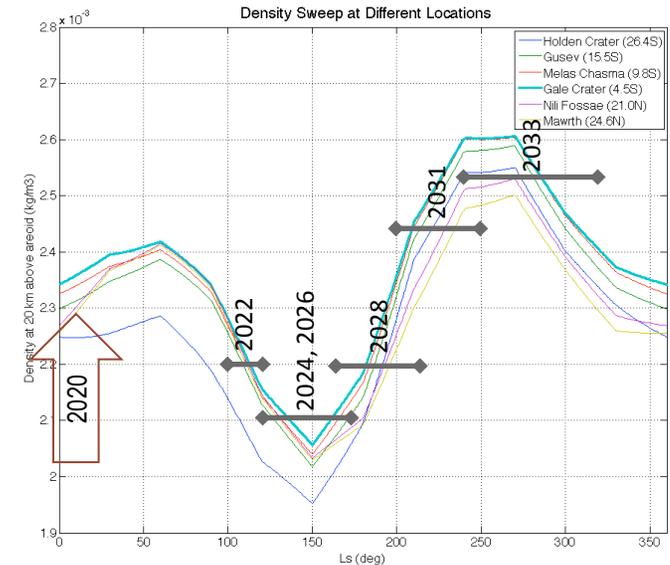
- ~2.5 km effect from pressure cycle variation

3 Parachute technology – increase in deploy Mach

- ~1.5-2 km effect, increasing Mach to 2.4 nominal
- **Note: area oscillations not modeled**

• Second order effects (≤ 0.5 km delta on landed elevation)

- Entry velocity (~50 m altitude per +0.1 km/s entry velocity)
- Entry FPA optimization (very small sensitivity)
- Time of day (~2-4% density variation = up to ~350 m impact)
- Landing site latitude (<6% density variation = up to ~500 m impact)
- Dust storms, Ls 180-330 (impact expected to be < 0.5 km)
- **Second-order variables were held constant in analysis



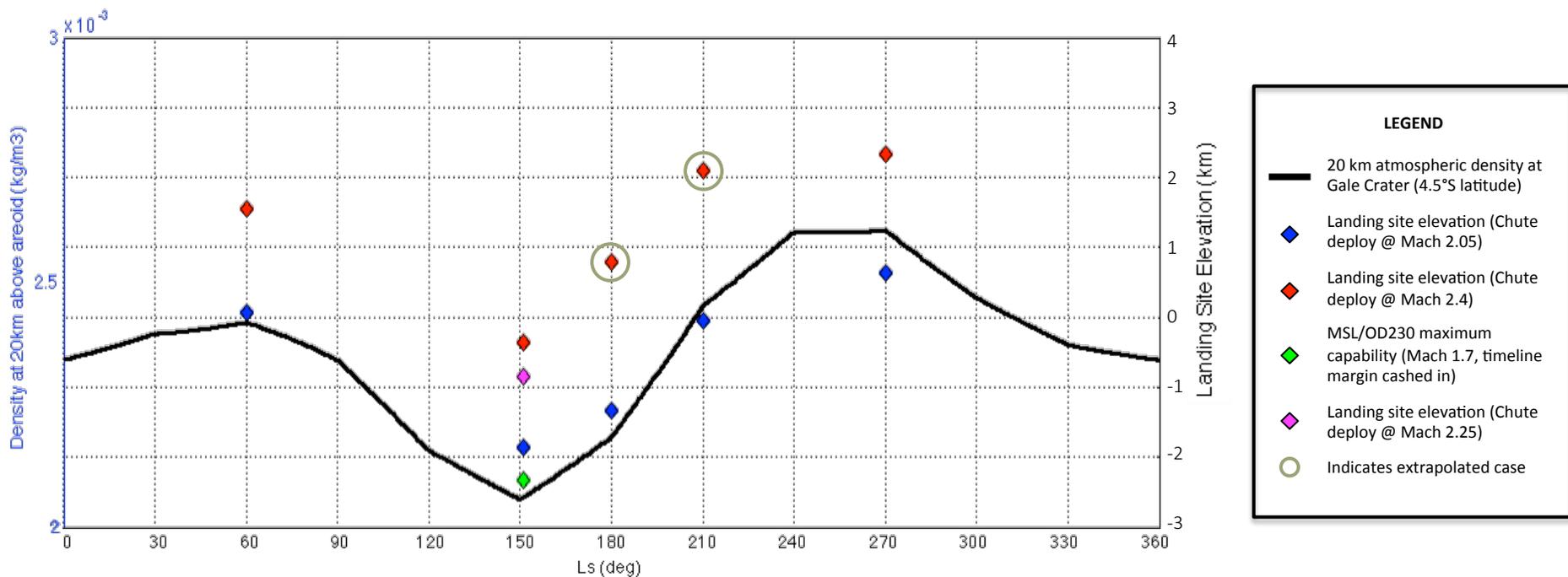
Landing Site Elevation Capability



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Mars Formulation

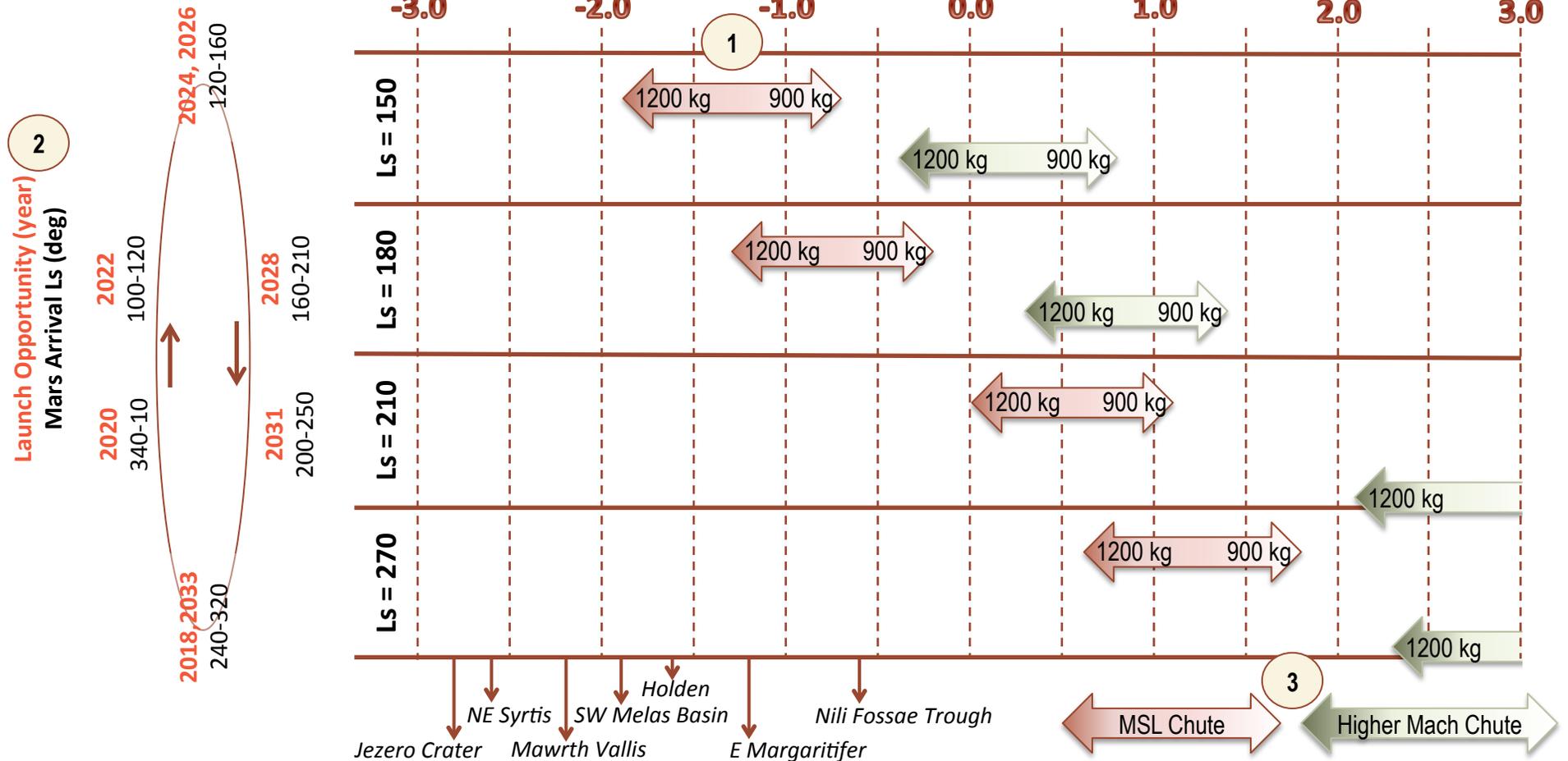
- Landing site elevation capability as a function of landing season
 - Blue points assume current parachute (DGB) capability
 - Red points assume higher Mach parachute capability
 - Study result partials applied to get cases beyond those run directly
 - Results have a $\sim \pm .5\text{km}$ error



Summary of Retrieval Altitude Considerations



Landed Altitude Capability, MOLA (km)



Conclusions



- There is sufficient fuel to land 1200 kg, but available development margin is thin
- Sites at or below ~ -1.0 km MOLA should be reachable by future SRL missions using existing EDL capabilities
 - Within capabilities for consecutive opportunities from 2028 – 2035
 - Ability to reach -1.0 km before 2028 will depend on landed mass required
 - Maximum possible elevation for a 1200 kg SRL is $\sim +0.5$ km
- Higher altitude landing sites (> -1.0 km MOLA), if chosen, can still be accessed but may require:
 - Delaying retrieval mission to opportunities with more favorable landing conditions (2028+), or
 - Adopting technologies to improve delivered mass (LDSD parachute), or
 - Investing in technologies to reduce landed mass requirements (esp. MAV)
- Other factors not considered in this study:
 - Landed precision
 - Landing site latitude
 - Design of future SRL rover



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Backup

MSL/M2020/SRL Comparison



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Mars Formulation

	MSL	Mars 2020 Baseline	Assumed SRL
Launch Vehicle	Atlas V 541	Atlas V 541 (pending LV selection)	TBD
Arrival Ls	150.6°	6° - 7°	Depends on Opportunity
Entry Mass	3152 kg	~3250 kg	~3550 kg
Landed Mass	899 kg	Up to 960 kg	1200 kg
Parachute Deploy Mach	1.75	Nominal: 2.05 Spread to: 2.2-2.3	TBD
Ballistic Coefficient	136 kg/m ²	140 kg/m ²	153 kg/m ²
Landed Elevation	-4.4 km (actual)	TBD	TBD
Max Elevation Capability	-1 km MOLA	+0.5 km MOLA	TBD
Landed Ellipse	<ul style="list-style-type: none"> Original: 25 km x 20 km Final: 19 km x 7 km 	<ul style="list-style-type: none"> 25 km x 20 km Final expected with range trigger: 13 km x 7 km 	TBD

Detailed Assumptions for Performance Simulations



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Mars Formulation

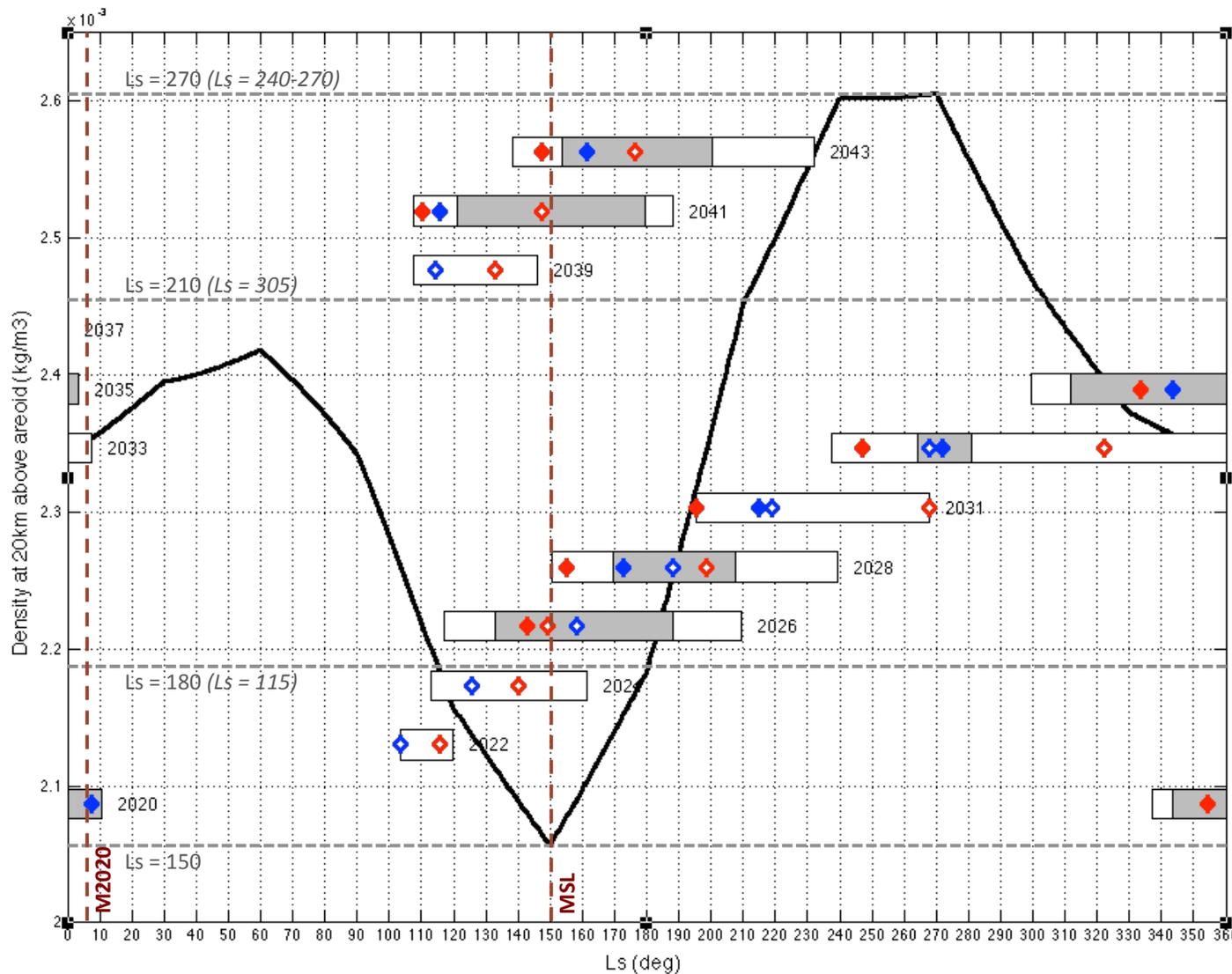
- Flew all simulation cases to Gale latitude/longitude and altitude with synthetic terrain
- Didn't increase mass of non-lander hardware (also didn't look at TPS)
- Entry vehicle fixed at MSL-like conditions (~ 6 km/s inertial, ~ 5.7 km/s atmosphere relative, EFPA = -15.5° , entry time of day ~ 3 PM)
- Seasonal dust assumptions, no dust storms considered
- "Engineering" winds applied for all cases, regardless of landing season
- Didn't tune entry guidance for landing season, but did tune guidance for higher Mach parachute deploy cases
- Didn't take advantage of potential higher subsonic Cd from a disksail parachute
- Didn't look at larger diameter chute
- Turned off area oscillations modeling (significant lien on high Mach results)
- Used a floor of 20 s of timeline margin

Liens Against Study Results



- Disabled area oscillations model
 - Results in severe angular rates and accelerations; magnified with greater exposure time due to high Mach deploys
 - Models based on one data point from BLDT
 - Upcoming LDSO tests may provide additional insight
- Did not increase mass of non-lander hardware
- Dust storms were ignored
 - Applicable to Ls 180 – 330
 - Impact on altitude performance expected to be < 0.5 km (density reductions less than previously believed)
 - Principal issue is changes in expected wind fields (landing precision)
- Fuel for TRN
 - Did not consider fuel impact for longer TRN/Multi-X divers

Arrival Ls for Future Opportunities ($C_3 < 15 \text{ km}^2/\text{s}^2$)



LEGEND

- 20 km atmospheric density at Gale Crater (4.5°S latitude)
- Arrival Ls range for $C_3 < 15 \text{ km}^2/\text{s}^2$ and at least one inertial entry velocity $< 7 \text{ km/s}$
- Arrival Ls range for $C_3 < 15 \text{ km}^2/\text{s}^2$ and at least one inertial entry velocity $< 6 \text{ km/s}$
- Minimum C_3 (Type I)
- Minimum C_3 (Type II)
- Minimum Inertial Entry Velocity (Type I)
- Minimum Inertial Entry Velocity (Type II)

Note:

- $C_3 = 15 \text{ km}^2/\text{s}^2$ corresponds to a launch mass of 4585 kg (~10% margin)
- 1200 kg landed mass requires launch mass of at least 4194 kg (assuming no additional mass required above MSL other than landed mass)